



COMPUTATION NOTE BOOK

43-648

Course UHF RECEIVER

Name PROJECT NOTEBOOK - STARTED 6-4-59

Del Mar Engineering Laboratories

LOS ANGELES, CALIFORNIA

PROJECT COMPUTATION RECORD

SERIAL NO.

Nº

62

#I

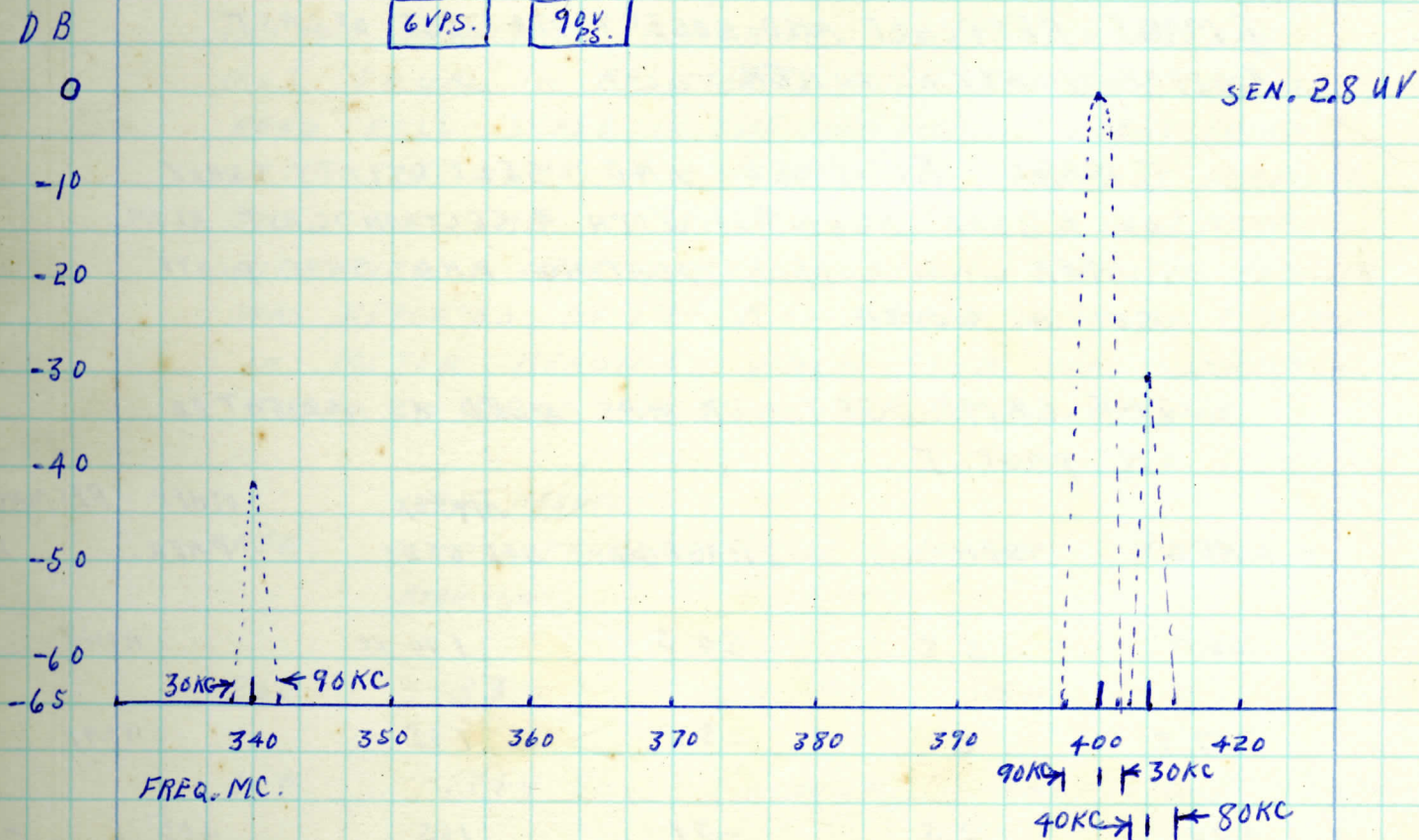
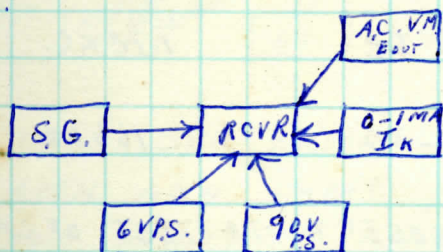
SELECTIVITY AND IMAGE RESPONSE CURVE ON R300A #31 RCVR.

6-8-59

OBJECT

TO DETERMINE THE SELECTIVITY AND IMAGE RESPONSES ON R300A WITH REGULAR 4 SECTION TUNER. ALL COVERS WERE IN PLACE AND RCVR. COVER ON.

THE EQUIPMENT USED WERE 6V POWER SUPPLY, MATTSOIN-CROWLEY POWER SUPPLY MODEL 113, HEWLETT-PACKARD 6080 SIG. GEN. BALLENTINE MODEL 314 AC. VOLT METER AND TRIPPLETT 420-PL 0-1 MA METER.



NOTE.

WITH THE SAME SET UP IMAGE REJECTION WAS MEASURED AT 260 AND 309.8 MC. THE IMAGE REJECTION AT 260 MC WAS -51 DB AND AT 309.8 IT WAS -47 DB. THERE WERE NO ^{OTHER} IMAGES ABOVE -65 DB AT ~~THE~~ EITHER FREQ.

II

IMAGE RESPONSE AND SELECTIVITY TEST OF R300A RCVR #31 WITH 3 SECTION TUNER 6-8-59

TO TEST THE SELECTIVITY OF R300A RCVR WITH 3 SECTION BRASS TUNER, NO COVER WAS USED ON TUNER OR RCVR.

THE SAME SET UP WAS USED AS INDICATED ON PAGE I.

FREQ.	SEN. (uv)	IMAGE (DB)	APPROX. SEL (65DB)	OTHER FREQ.	RESPONSES DB
260	3	-34	170KC	NONE	
309.8	4	-32	172KC	390 440	-64 -53
400	1.6	-30	166KC	403	-30

III

IMAGE RESPONSE AND SELECTIVITY TEST OF CAST COPPER PLATED TUNER.

IMAGE RESPONSE AND SELECTIVITY CURVE OF R300A RCVR #31 WITH 4 SECTION CAST ALUM. TUNER WITH COPPER PLATING AND BASE PLATE USED AS COVER.

THE SAME SET UP WAS USED AS INDICATED ON PAGE I.

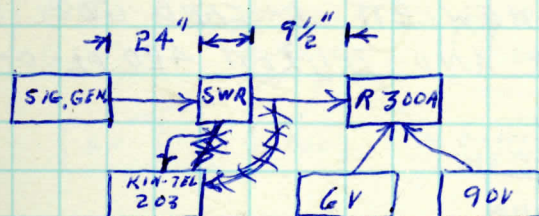
FREQ	SEN. (uv)	IMAGE (DB)	APPROX. SEL. 65DB	OTHER FREQ	RESPONSES DB
260	5.8	-54.5	170 KC	NONE	
309.8	6	-53	168	NONE	
400	2.5	-51	165	403	-38

IMPEDANCE AND STANDING WAVE RATIO

6-9-59

TO DETERMINE THE BEST IMPEDANCE MATCHING TO THE R300A RCVR.

THE HEWLETT-PACKARD 608C SIGNAL GEN., KIN-TEL MODEL 203, 6V POWER SUPPLY, MATTSON-CROWLEY MODEL 113 POWER SUPPLY AND STANDING WAVE RATIO BRIDGE. RG-58 A/U COAXIAL CABLE WAS USED.



THE SWR BRIDGE WOULD NOT BALANCE OUT BETWEEN THE OPEN AND SHORT POSITIONS AS INDICATED IT SHOULD IN THE AMATEUR'S HANDBOOK. SO R_1 AND R_2 ARE NOT EQUAL IN RESISTANCE. WHEN THE SWR WOULD READ FULL SCALE IN THE OPEN POSITION. EVERY THING LEFT THE SAME A 47 Ω RESISTOR WAS PUT ACROSSED THE COAX THE METER WOULD ZERO OR VERY NEAR INDICATING A NEAR PERFECT MATCH. THEN THE RESISTOR WAS REPLACED BY THE R300A RCVR. WITH NO CHANGE IN METER READINGS WHEN RCVR WAS CORRECTLY TUNED TO SAME FREQ. AS SIGNAL GENERATOR.

FREQ.	INPUT NEEDED			
	TO OBTAIN FULLSCALE READING	SCALE	47 Ω LOAD	RCVR.
260	.83 V	0-3 MV	.06 MV	0
400	.74 V	0-100 mV	5 mV	6 mV

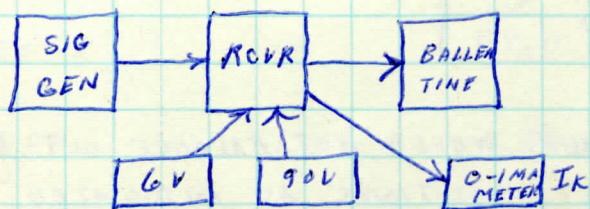
IF SWR BRIDGE IS NEAR CORRECT THE RCVR. IS ABOUT THE SAME AS 47 Ω LOAD RESISTOR. AND SEVERAL DIFFERENT VALUES OF RESISTANCE WERE TRIED.

JFD CHANGE IN TUNER

6-10-59

TO REDUCE THE TUNER SIZE A DIFFERENT JFD CAPACITOR WILL HAVE TO BE USED IN PLACE OF JFD VCIG TO ELIMINATE THE LONG EXTERNAL SHAFT FOR ADJUSTING. IN THE OSC. SECTION.

RCVR #31 WAS USED TO RUN TEST TO MAKE SURE TUNER COVERED THE FREQ. RANGE WORKED PROPERLY. THE 6V POWER SUPPLY, MATTSON-CROWLEY 113 POWER SUPPLY, ~~HEWLETT~~ HEWLETT-PACKARD 608C SIG. GEN., BALLENTINE 314 AND TRIPKETT 420 PL 0-1 MILL METER.



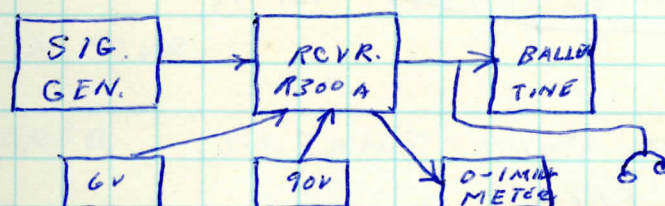
A JFD V620G WAS USED, IT HAD THE RIGHT CAP RANGE .8-8.5 IT WAS PARALLELED WITH A 1 μ f TLO CAP. AND A COIL WITH 3 turns WAS USED TO COVER THE FREQ. RANGE OF 230 TO 370 MC WHICH IT DID. WITH COVER OFF IT COVERED A RANGE FROM 190 TO 438 MC.

NEW TUNER FOR R300A

6-11-59

TO FIND A BETTER TUNER FOR FUTURE RCVR.
WITH BETTER SEN., IMAGE REJECTION AND NO RESPONSES

EQUIPMENT USED FOR TESTING R300A #31 RCVR.
6V POWER SUPPLY, MATTSOK-CROWLEY 113 POWER SUPPLY, HEWLETT-
PACKARD 608C SIG GEN. BALLENTINE 314 AND TRIPPLETT 420PL
0-1 MILL METER.



NEW TUNER $\frac{1}{2}$ " LONGER THAN PRODUCTION WITH
COUPLING LOOPS $\frac{1}{2}$ " LONGER THAN " MODEL
WITH MIXER COUPLING CLOSE $\frac{1}{32}$ " spacing. ALL OTHER
COUPLING SPACES NORMAL.

TUNER CHECK OUT BEFORE INSTALLING IN RCVR.

	MILL-VOLTS	RESPONSES
360 MC	185	375 MC .03 MV
300	170	294 MC .12 MV
400	130	NONE

TUNER AFTER INSTALLATION IN RCVR.

FREQ	SEN.	IMAGE	RESPONSES ABOVE 65 DB.
260	1.6	-50	430-62 DB
309.8	1.8	-44	295-61 DB, 297-38 DB 450-61 DB
400	5	-14	NONE

NOTE: WITH NORMAL COUPLING IN MIXER STAGE.

400	8	-14	NONE
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NOTE: GRAPHS ON FOLLOWING PAGES

SEN. CURVE

μV
SEN. A 80%
MOD.

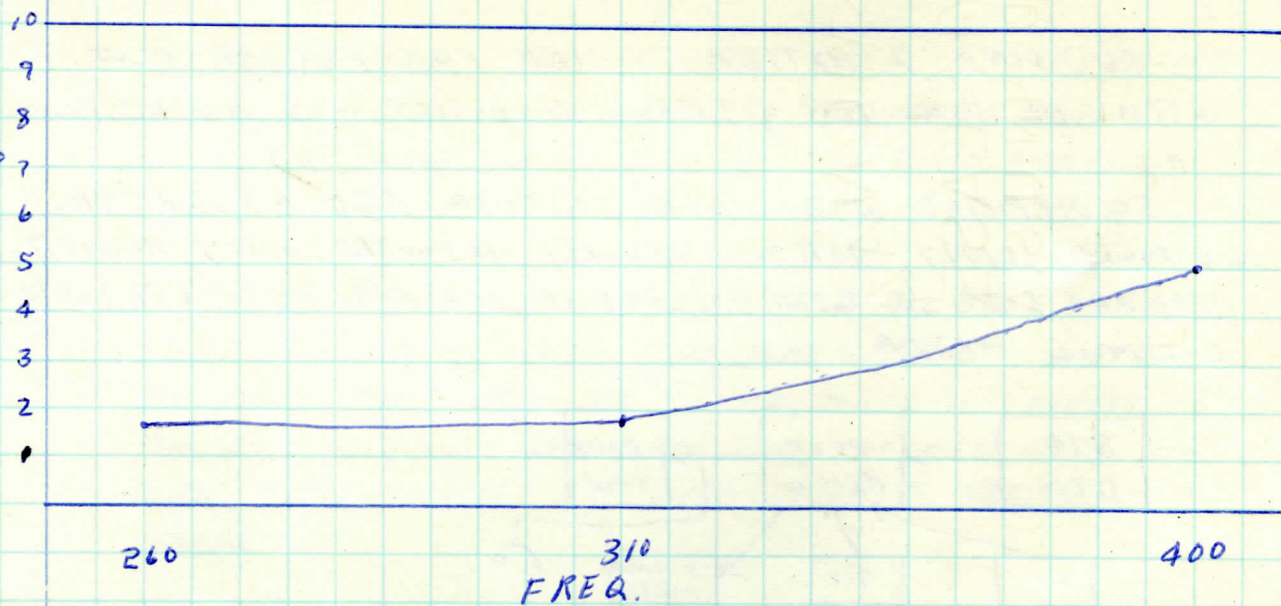
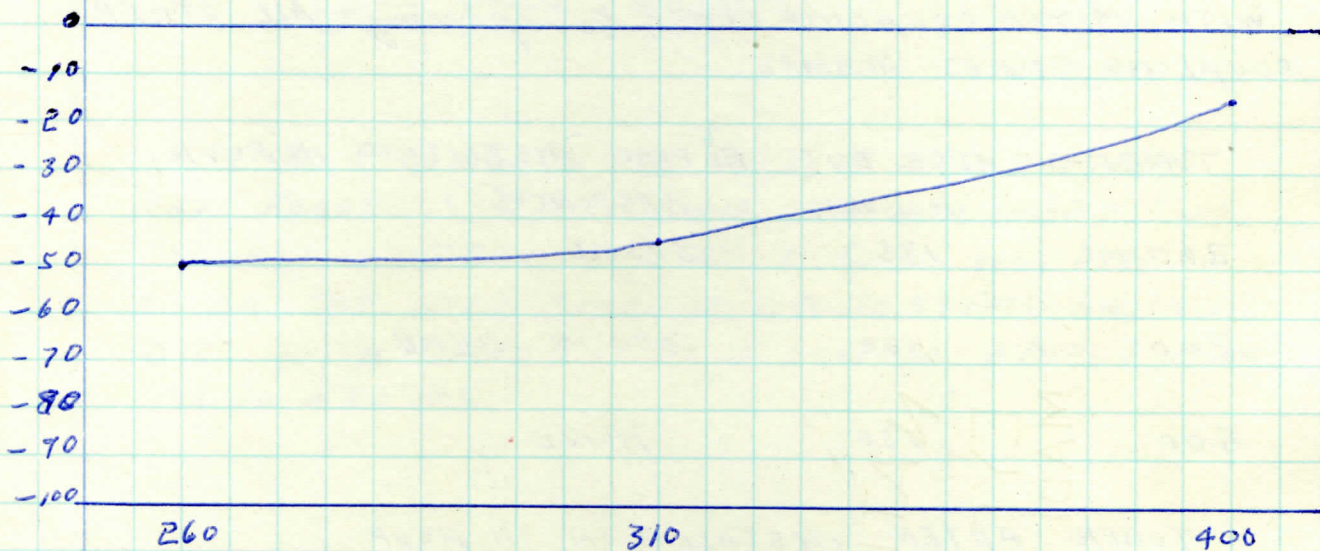


IMAGE REJECTION CURVE

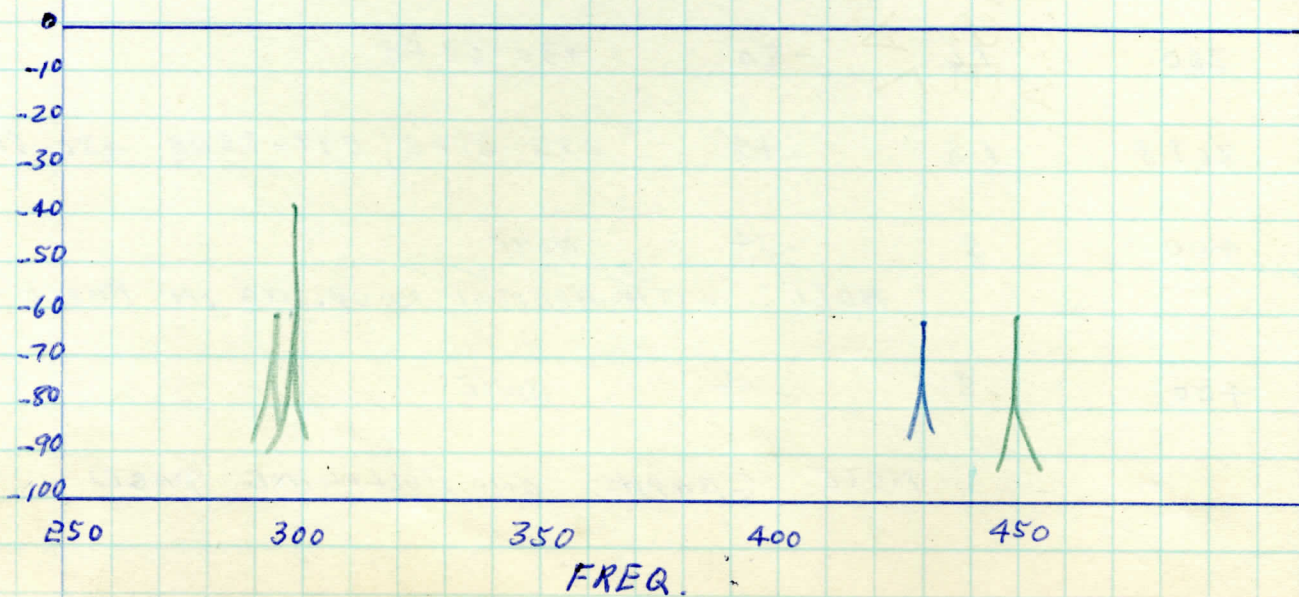
DB



SPURIOUS RESPONSES

DB

260 - λ
309.8 - λ
400 - λ



SE
80%

NEW TUNER WITH COUPLING LOOPS $\frac{1}{4}$ " ^{LONGER} ~~SHORTER~~ 6-15-59
THAN #31

TO CHECK OUT NEW TUNER WITH COUPLING SHORTENED
 $\frac{1}{4}$ " AND ~~EVERY~~ EVERYTHING ~~THE~~ THE SAME AS BEFORE
USING NORMAL COUPLING BETWEEN ALL STAGES.

THE SAME EQUIPMENT USED AND SET UP AS USED
ON PAGE 5.

TUNER CHECK OUT BEFORE INSTALLING
IN RCVR.

FREQ	SIG. INPUT	RESPONCES
260	275	266 -.03
330	235	341 -.07
400	135	407.5 -.32

AFTER INSTALLATION IN RCVR. FOR NORMAL
CHECK OUT.

FREQ.	SEN.	IMAGE	RESPONCES ABOVE -65 DB
260	3	-51	431 -63 DB
309.8	3	-50	NONE
400	1.8	-43	403 -41 DB

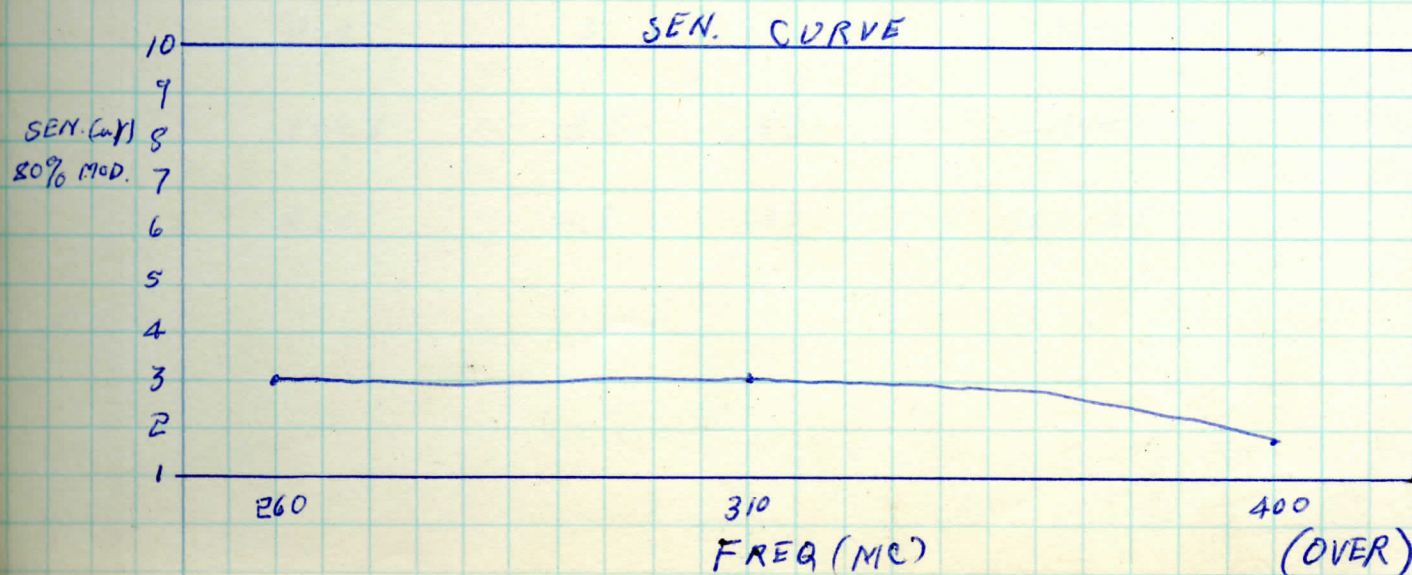
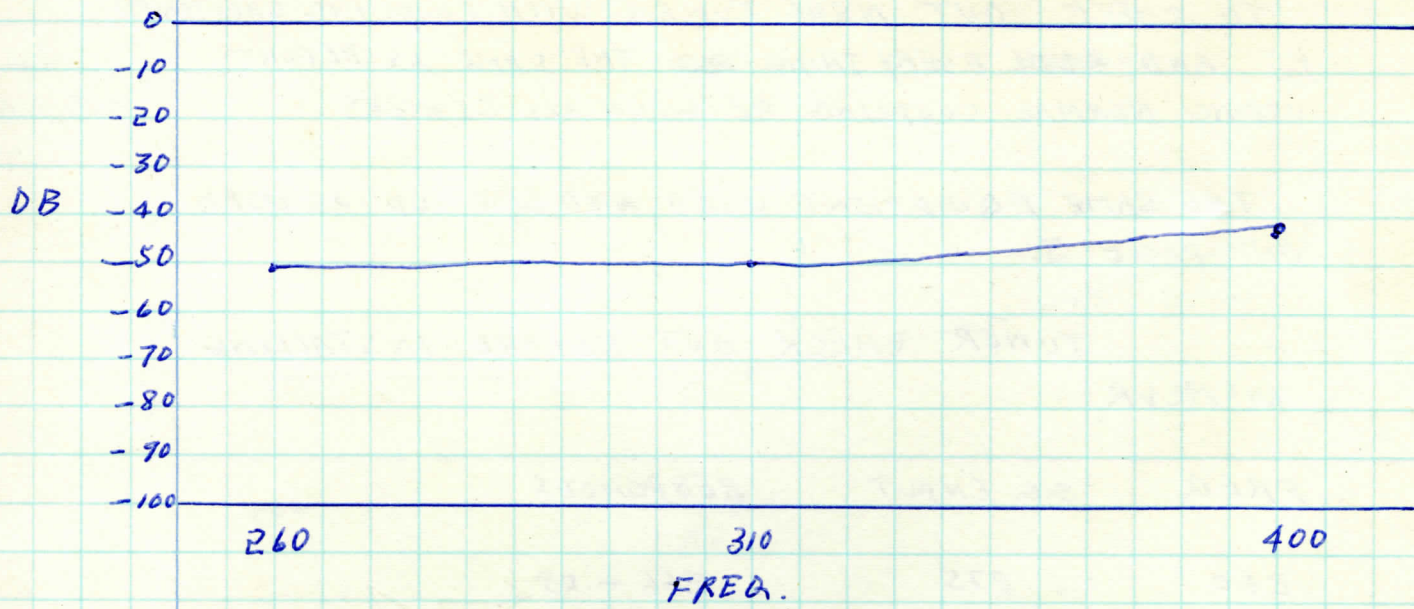
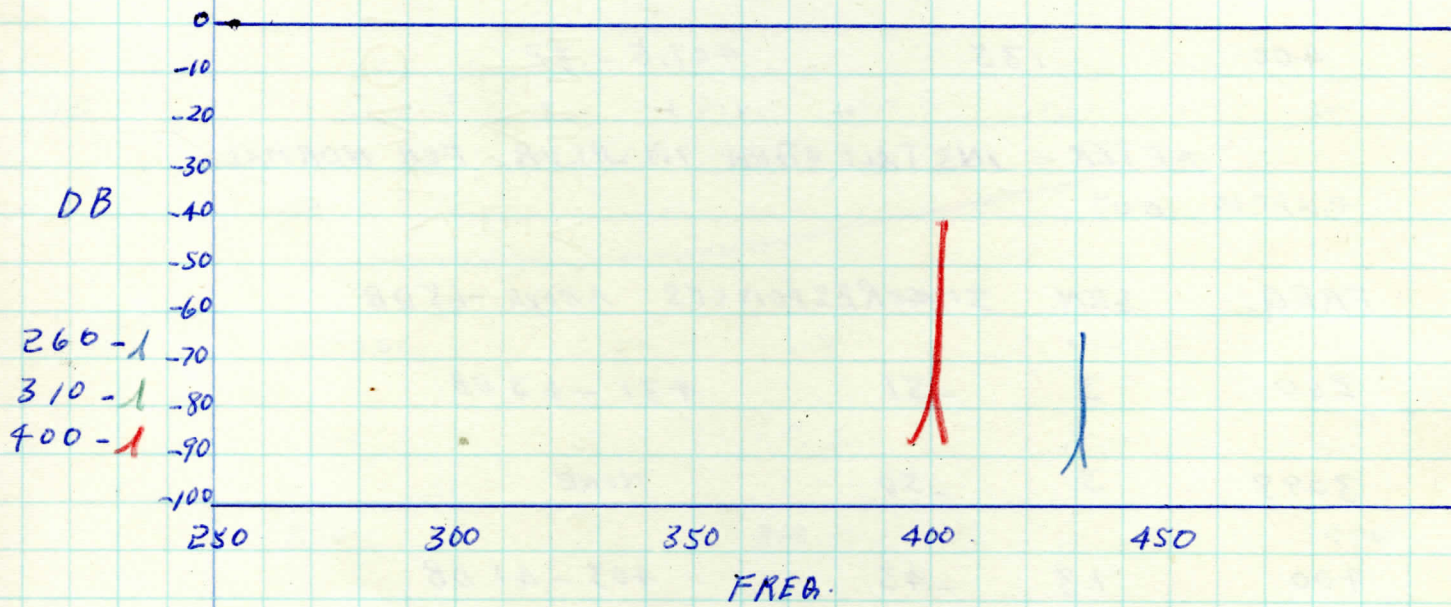


IMAGE REJECTION ~~GRAPH~~ CURVE

SPURIOUS RESPONSES



6-16-59

CHECK OUT OF NEW TUNER

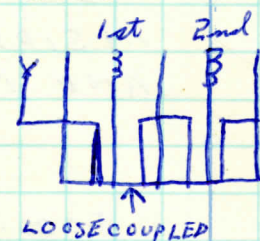
THE SAME EQUIPMENT WAS USED AS INDICATED ON PAGE 5.

THE TUNER WAS $\pm 31 + \frac{1}{2}$ " LONGER ALL COUPLING LOOPS WERE $\frac{1}{4}$ " LONGER AND $\frac{1}{2}$ " LONGER ON OSC AND MIXER.

(MC) FREQ	(dV) SEN.	(DB) IMAGE	RESPONCES
260	2.8	-51	NONE
309.8	2.5	-49	NONE
400	2.2	-48	403-26 DB

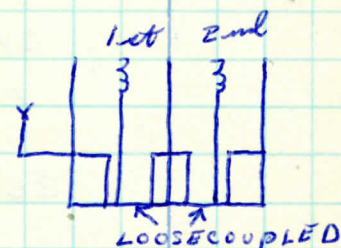
SAME AS ABOVE WITH 1st. R.F. STAGE LOOSE COUPLED TO 2nd RF STAGE

400	1.6	-41	403-28
309.8	2	-52.5	NONE
260	2.8	-54	NONE



SAME AS ABOVE WITH LOOSE COUPLING BETWEEN 1st and 2nd R.F. STAGES.

260	3	-55	NONE
309.8	2.5	-52	NONE
400	1.8	-43	403-27



CHECK OUT OF #31 TUNER $\frac{1}{2}$ " IN LENGTH 6-17-5

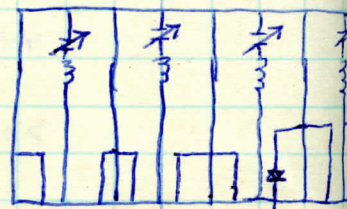
SAME EQUIPMENT AND SET UP USED AS INDICATED ON PAGE 5.

LOOSE COUPLING USED BETWEEN 1st AND 2nd RF stages AND MIXER LOOSE COUPLED.



FREQ.	SEN.	IMAGE	RESPONCES
260	3.5	-56	NONE
309.8	2.7	-53	NONE
400	2	-43	403-30

SAME AS ABOVE BUT WITH MIXER CRYSTAL INSIDE TUNER. AND COUPLING LOOP BETWEEN OSC AND MIXER $\frac{1}{2}$ " LONGER THAN #31 TUNER.



400	2.3	-49	403-27
309.8	2.7	-53	NONE
260	2.6	-58	NONE

SAME AS ABOVE BUT WITH COVER SOLDERED IN PLACE ON 1st RF STAGE.

260	2.6	-57	NONE
309.8	2.6	-54	NONE
400	1.8	-49	403-28 dB

17-51

CHECK OUT OF [#]31 TUNER + 1/2"

6-18-59

TO DETERMINE IF RESPONSE AT 403 IS FROM TUNER.

EQUIPMENT USED R300A RCVR, 6V POWER SUPPLY
MATTSON-CROWLEY 113 POWER SUPPLY, HEWLETT-PACKARD
608C AND 608D SIG. GENERATORS, BALLENTINE 314
AND TRIPPLET 420PL 0-1 MILL METER.

OSC. IN RCVR. WAS DISABLED AND 608D SIGNAL
GEN. WAS CONNECTED TO OSC. SECTION OF TUNER BUT
PUT OF SIGNAL GEN. COULD NOT BE ADJUSTED WELL
BUT THE PROPER AMOUNT OF CRYSTAL CURRENT
WAS OBTAINED.

FREQ	SEN.	IMAGE	RESPONCES
400	2.7	-48	NONE
309.8	3.7	-55	NONE
260	5	-61	NONE

THE RESPONSES WERE COMING FROM LOCAL OSC.

THE LOCAL OSC. WAS HOOKED UP AND CHECKS
WERE RUN AT THE FOLLOWING FREQ.

XTAL. FREQ	FREQ	SEN.	RESPONCES	7 TH HAR. OF XTAL.	$f_s - f_o$
61.75	400	1.8	403-28 DB -70	432-30 = 402	3
58.5	381	2	379-33 DB -62	409-30 = 379	-2
51.110	336.6	2.5	328-46 DB	357.7-30 = 327.7	-8.6
50.5	333	2.7	324-61 DB	353-30 = 323	-9
46.633	309.8	3	312-77 DB	326-15 = 311	+2.2
38.33	260	2.7	NONE		

TUNER CHECK OUT. #31 TUNER + $\frac{1}{4}$ "

6-22-59

A TUNER $\frac{1}{4}$ " LONGER THAN #31 AND THE COUPLING LOOPS ARE THE SAME AS #31 TUNER WITH OSC. IN PUT IN LINE WITH OTHER LOOPS.

THE SAME EQUIPMENT AND SET UP WAS USED ON PAGE #5.

(MC) FREQ	(μ V) SEN.	DB IMAGE	RESPONCES
400	2	-60	403-42
309.8	4	-47	NONE
260	5.5	-51	430-57

SAME AS ABOVE BUT WITH OSC. INPUT MOVED $\frac{3}{8}$ " LONGER.

260	3.5	-52	430-60
309.8	3.4	-46	NONE
400	2.5	-44	403-42

SAME AS ABOVE WITH COUPLING LOOP MOVED TO POSITIONS TO OBTAIN GREATER SEN. AND MORE IMAGE REJECTION AND ELIMINATE SPURIOUS RESPONCES DOWN. OSC. INPUT WAS MOVED TO $\frac{1}{2}$ " LONGER THAN #31

400	4.7	-42DB	403-28DB
309.8	4	-50DB	NONE
260	3.3	-56DB	NONE

THIS TYPE TUNER $\frac{1}{4}$ " LONGER WAS DISCONTINUED BECAUSE GOOD RESULTS COULD NOT BE OBTAINED IN REGARD TO SEN., IMAGE, AND RESPONCES.

22-59

NEW TUNER TO BE USED

6-23-59

THE TUNER THAT WILL BE USED HAS THE FOLLOWING COUPLING AND SIZE.

TUNER IS $\frac{1}{2}$ " LONGER THAN #31 PRODUCTION MODEL
ALL COUPLING LOOPS ARE $\frac{1}{4}$ " LONGER THAN #31 EXCEPT
THE COUPLING LOOP BETWEEN OSC. AND MIXER WHICH
IS $\frac{1}{2}$ " LONGER THAN #31 WITH OSC. INPUT $\frac{1}{2}$ " LONGER
THAN #31 TUNER.

THE COUPLING BETWEEN THE 1st AND 2nd RF. STAGES
ARE LOOSE COUPLED TO BRING IMAGE DOWN. AND
MIXER CRYSTAL IS PLACED IN SIDE TUNER.

THE FOLLOWING MEASUREMENTS WERE MADE
USING THE SAME SET UP AS INDICATED ON PAGES.

(MC)	(μ V)	DB	(FREQ) (DB)
FREQ	SEN.	IMAGE	RESPONCES
260	2.6	-57	NONE
309.8	2.6	-54	NONE
400	1.8	-49	403-28DB

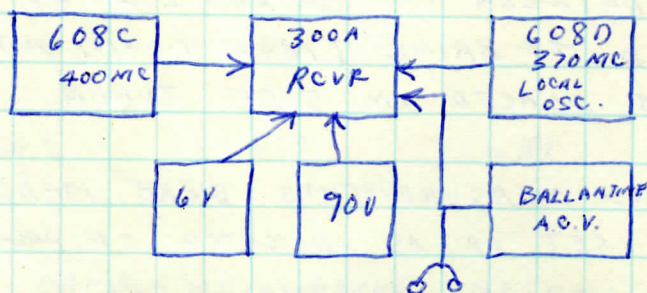
NOTE: AN ALUM. CASTING WILL MADE TO
SEE IF IT WILL WORK IN PLACE OF .015 BRASS.

CHECKS TO SEE IF RESPONSES ARE
COMING FROM TUNER OR OSC.

6-23-59

THE LOCAL OSC. WAS DISCONNECTED AND
608D WAS USED AS LOCAL OSC.

EQUIPMENT USED HEWLETT-PACKARD 608C AND
608D SIG. GEN., MATISON-COWLEY 113 POWER
SUPPLY, 6V REGULATED POWER SUPPLY, BALLANTINE AC. METER
AND TRIPLETT 42403 PL.



WITH RCVR TUNED TO 400 MC AND 370 MC
FREQ INJECTED INTO OSC. STAGE OF TUNER. THE
FOLLOWING RESPONSES.

FREQ	SEN.	IMAGE	RESPONCES
400 MC	2.2 μ V	-49 DB	401.5 - 92 DB
			404.5 - 91 DB

USING THE SAME SET UP AS ABOVE EXCEPT SIGNAL
FOR LOCAL OSC. THE SIGNAL WAS INJECTED INTO
GRID OF 5703 AND THE FOLLOWING RESULTS WERE OBTAINED

FREQ	SEN.	IMAGE	RESPONCES
400 MC	3.1 (μ V)	-49 DB	401.5 - 82 DB
			404.5 - 81 DB

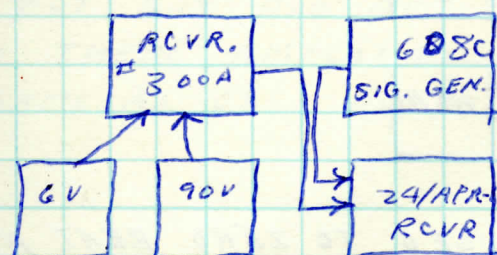
FROM CHECK OF FREQ COMING LOCAL OSC.

6-23-59

RCVR. WAS TUNED TO 400 MC USING 61.750 MC CRYSTAL

EQUIPMENT USED. HEWLETT-PACKARD 608C, MX-24/APR-1 RADIO RCVR., MATTHEWSON-COWLEY 113 POWER SUPPLY, AND 6V REGULATED POWER SUPPLY.

THE RCVR. WAS TUNED TO 400 MC AND THE MX-24/APR-1 WAS USED AS A ~~DET~~ DETECTOR AND THE HEWLETT-PACKARD 608C WAS USED AS AN OSC. TO ZERO BEAT AGAINST THE FREQ. FROM THE OSC. IN RCVR #300A.



THE FOLLOWING FREQ. WERE FOUND
WITH 6AF4A WITH 6AF4A REMOVED
(HARMONIC) FREQ. (MC) FREQ. MC.

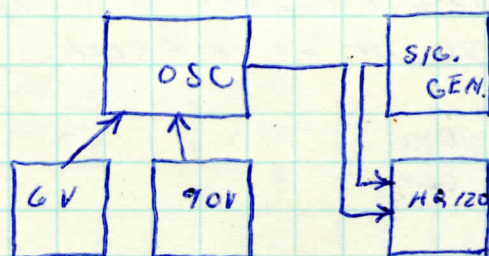
2	123.6	123.6 (2 RESPONSES)	(NOTE) TOO CLOSE TO MEASURE
3	185.5 (2 RESPONSES)	164	(NOTE) TOO CLOSE TO MEASURE
4	247.5	171	
5	309	185.5 (2 RESPONSES)	(NOTE) TOO CLOSE TO MEASURE
	323	247.5	
	330	309	
6	370	323	
	380	341.5	
	420	370	
	460	380	
		420	
		460	

NOTE: THESE DOUBLE RESPONSES COULD BE TUNED OUT BY ADJUSTING THE LAST OSC. STAGE.

CHECK OF 6III STAGE FOR RESPONSES

TO DETERMINE WHAT FREQ. IF ANY ARE COMING FROM THE 6III STAGE OF OSC. THE OSC. WAS REMOVED FROM RCVR. AND S703 STAGE WAS DISABLED.

THE FOLLOWING EQUIPMENT WAS USED HEWLETT PACKARD 6080 SIG. GEN., HAMMARLAND HQ-120 MATTSON COWLEY POWER SUPPLY AND 6V REGULATED POWER SUPPLY.



THE 6080 WAS USED TO ZERO BEAT AGAINST THE SIGNAL FROM OSC. AND HQ 120 WAS USED AS A DETECTOR.

WITH 61.75 CRYSTAL IN OSC THE FOLLOWING FREQ WERE FOUND.

12.1, 15.15, 15.65, 15.9, 16.55, 17.75, 19.95, 20.85, 21.15, 21.75, 22.7, 25.4, 27.3, 28.1, 29, 29.95, 30.2, 30.65, 30.85 AND 30.9

WITH 58.5 CRYSTAL

14.78, 18.25, 19.8, 19.85, 20.0, 21.0, 23.75, 23.95, 25.45, 29.45, 29.51, 29.55, 29.7, 29.75 AND 29.95.

WITH 51.110 CRYSTAL

7.4, 25.8, 25.95, 26.18 AND 26.25

ALL THESE FREQ. WERE FOUND BELOW 31 MC WHICH WAS THE UPPER LIMIT OF HQ 120 RCVR.

CHECK OF OSC. WITH 680- Ω RES.
REPLACED WITH 470- Ω RESISTORS.

6-25-59

SAME SET UP WAS USED AS INDICATED ON PAGE #16

R202 AND R204 WERE CHANGED TO 470- Ω RES.
AND THE FOLLOWING FREQ WERE FOUND WITH
51.110 CRYSTAL IN OSC.

7.4 , 25.8 25.95 26.18 AND 26.25.

THESE RES. CHANGES ONLY LOWERED THE OSC.
OUT PUT. BUT DID NOT CHANGE ANY FREQ PRESENT.
ONLY THERE AMPLITUDE WHICH APPEARED TO BE ^{LOWERED} ~~THE SAME~~
THE SAME AS OSC. OUTPUT.

CHECK OF OSC. WITH 680- Ω RES. BACK IN OSC.
AND A 68- Ω RES. ~~WAS~~ PLACED IN GRID LEAD TO
GROUND.

SAME EQUIPMENT USED AS INDICATED ON PAGE #16
58.5 CRYSTAL WAS USED. AND TEST POINT 1 = .24 MA

THE FOLLOWING FREQ. WERE FOUND.

15.1 , 17.97, 18.25, 19.8, 19.85, 20.0 20.1 23.75
23.75, 25.45, 29.45, 29.51, 29.55, 29.75, 29.95

THE AMPLITUDE OF THESE FREQ. WERE LOWERED AND
THREE OTHER CRYSTALS WERE USED TO FIND
~~THE~~ TEST POINT 1 READINGS.

FREQ MC	TP-1
61.75	.24
58.5	.24
50.5	.27
38.32	.27

THE 68- Ω RESISTOR HAS LEVELED OUT THE
READINGS OVER THE ENTIRE FREQ. RANGE OF OSC.

OSC. CHECKS WITH CAP. CHANGES

6-26-51

TO TRY AND ELIMINATE UNWANTED FREQ.
WITH CAP. CHANGES. C204 = 25 μ mf.

THE SAME EQUIPMENT AND SET UP WAS USED
AS INDICATED ON PAGE 16.

C204 = 20 μ mf AND CRYSTAL FREQ = 58.5 TP-1 = .3

FREQ. PRESENT WERE 29.95, 29.75, 29.55, 29.51,
29.45, 25.45, 23.95, 23.75, 20.1, 20.0, 19.85, 19.8,
18.25, 17.97 AND 15.1.

NEXT A 15 μ mf CAP. WAS USED IN PLACE OF 25 μ mf
C-204. TP-1 = .23.

FREQ. PRESENT WERE THE SAME AS ABOVE
BUT WITH LOWER ~~AMP~~ OUTPUT.

NEXT A 33 μ mf WAS USED IN PLACE OF THE 25 μ mf.
TP-1 = .32

FREQ. PRESENT WERE THE SAME AS ABOVE.

NEXT A 39 μ mf WAS USED IN PLACE OF THE 25 μ mf.

THE OSC. COULD NOT BE PEAKED UP TO WORK
~~PROPERLY~~ PROPERLY.

OSC. CHECKS WITH ACOIL ACROSSED XTAL6-29-30

A 1uh COIL WAS PLACED ACROSSED THE CRYSTAL TO SEE IF IT ELEMINATED THE UNWANTED FREQ.

THE SAME SET UP WAS USED AS INDICATED ON PAGE 16.

A 58.5 CRYSTAL WAS USED WITH A 1uh COIL PLACED ACROSSED IT.

THE FOLLOWING FREQ. WERE FOUND.

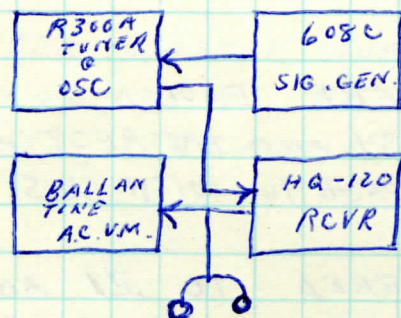
29.95, 29.75, 29.55, 29.51 AND THE REST WERE THE SAME AS BEFORE ON PAGE 16 WITH 58.5 XTAL.

TP-1 OUTPUT WAS LOWERED TO .21 AND OSC WAS INSTALLED IN R300A RCVR. AND RETUNED TO 400 MC. THE RESPONSE WAS STILL THERE AT 403 MC ONLY 31 DB DOWN. FOR THIS TEST THE SAME SET UP WAS USED AS INDICATED ON PAGE 5.

CHECK TO SEE IF DETECTOR IS EFFECTING 6-30-59
OR CAUSING RESPONSES

TO REMOVE DETECTOR AND DEMODULATOR FROM
RCVR. AND USES HQ-120 RCVR. HOOKED TO MIXER
CRYSTAL THROUGH COAXIAL CABLE AND USE AS A DETECTOR.

EQUIPMENT USED HEWLETT-PACKARD 608C, HAMMARLAND
HQ-120 RCVR, BALLANTINE 314 AC VOLT METER



THE HQ-120 WAS ZERO BEAT TO 30 MC WITH 608C
SIGNAL GEN., THE BALLANTINE WAS USED TO MEASURE SIGNAL
AMPLITUDE. THE FOLLOWING FREQ. WERE FOUND RCVR TUNED
TO 400 MC.

FREQ	INPUT	OUTPUT	
400	315 mV	IVAC	
400.873	140 mV	IVAC	MAIN SIGNAL
402.5	10.5 mV	IVAC	
403	30 mV	IVAC	
340	14 mV	IVAC	IMAGE

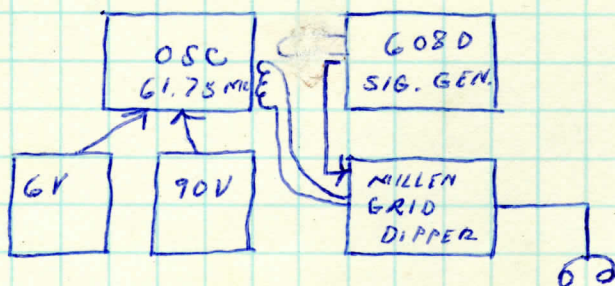
THE RESPONSES ARE ~~PRODUCED~~ PRODUCED BY
THE LOCAL OSC. WITH THE DETECTOR REMOVED
THE RESPONSES ARE IN THE SAME PLACES. SEVERAL
DIFFERENT VALUES OF COUPLING CAP. WERE USED
IN THIS TEST BUT THEY WOULD INCREASE OR
DECREASE THE RESPONSES AND THE MAIN SIGNAL
WOULD FOLLOW.

CHECK OF OSC. ALONE. FROM 30 MC AND UP

7-1-59

A CHECK ~~FOR~~ FOR DIFFERENT FREQ. WAS MADE WHEN THE OSC. TUNED TO 61.75 MC AND THE 5703 STAGE NOT OPERATING.

EQUIPMENT USED HEWLETT-PACKARD 608D, MILLER GRID DIPPER, 90V BATTERIES AND 6V REGULATED SUPPLY. THE 608D SIG. GEN. WAS USED TO ZERO BEAT AGAINST THE GRID DIPPER WHICH WAS USED AS A DETECTOR.



FREQ. FOUND WERE 61.75 ANOTHER RESPONSE 2.5 MC HIGHER

" " " 123.6 " " 2.5 MC "

" " " 185.5 " " 2.5 MC "

THESE RESPONSES WERE VERY STRONG BUT WERE NOT UP TO MAIN SIGNAL LEVEL.

7/23/59

At Tuner After Blasting interior + plating
with Silver. Mixer diode inside Mixer Section.
Normal Coupling.

Freq.	Sens.	Image	Responses
400	2	-58db	99.5 - 62db 133 - 59db 200 - 53db 402 - 62db 403 - 39db
309.8	2.5	-50db	103 - 57db 154.5 - 52db
260	2.7	-55db	65 - 60db 86.5 - 59db 129 - 51db

L 202 wound opposite direction, Same As
Above otherwise.

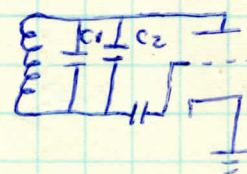
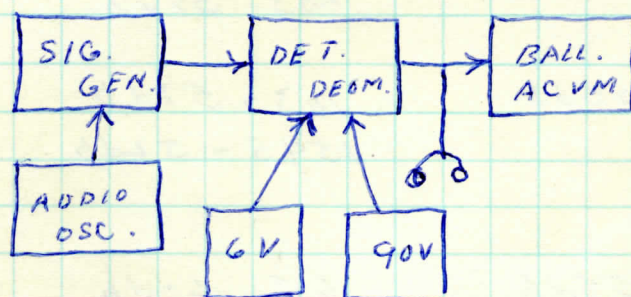
260	4.5	-55db	65 - 59db 86.5 - 54db 129 - 50db
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COLD TEST: R300A DETECTOR AND DEMODULATOR

7-28-59

TO DETERMINE THE AMOUNT OF FREQ
CHANGE AND ELIMINATE SAME.

EQUIPMENT USED HEWLETT PACKARD 608D
SIG. GEN., BALLANTINE 314 AC. VOLT METER,
6V POWER SUPPLY, 90V BATTERIES AND SIMPSON
MODEL 388 THERM.-O.-METER AND HEATH KIT AUDIO
OSC. MODEL AQ-1.



$C_1 = 27 \mu\text{f TCO}$
 $C_2 = 1.5 \mu\text{f TCO}$

NO. 1 DETECTOR, NO. 24 DEMODULATOR

FREQ (MC)	AMB. TEM.	UNIT. TEM.	SEN (uv)	AUDIO FREQ. (Hz)
30.000	84°	84°	1.6	1030
30.000	60°	60°	1.6	1000
30.000	40°	40°	1.6	985
30.000	20°	21°	1.6	970
29.996	10°	20	1.6	970
29.990	-20°	-18°	1.6	980
29.990	-40°	-37°	1.6	990
29.987	-50°	-46°	1.6	990
29.984	-65°	-65°	1.6	1000

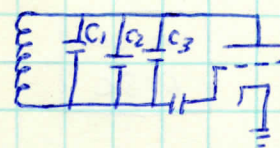
59

COLD TEST R300A DETECTOR AND DEMODULATOR

7-29-59

TO ELIMINATE FREQ. DRIFT WITH TEMP. CHANGE
 SAME EQUIPMENT AS USED ON PAGE 28.

NO. 1 DETECTOR AND NO. 24 DEMODULATOR

 $C_1 = TCO - 27 \mu f$ $C_2 = TCO - 1 \mu f$ $C_3 = TC3 - 1 \mu f$

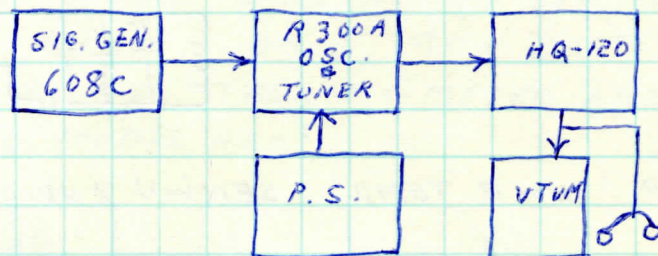
FREQ. (MHz)	AMB. TEMP.	UNIT. TEMP	SEN. (uV)	AUDIO FREQ. (Hz)
30,000	77°	81°	1.6	1030

OSC. CHECKS

8-10-59

TO TRY AND ELEMINATE RESPONSES COMING FROM OSC.

EQUIPMENT USED HEWLETT PACKARD 608C, HAMMARLAND HQ-120 RECEIVER AND HEATHKIT VTVM V-7A.



OSC. NORMAL WITH SHIELD BETWEEN 6111 AND 5703 STAGES.

NOTE: ALL READINGS ARE ON DBM SCALE OF 608C

FREQ. SEN. RESPONSES

400 85 402.5 - 31 DB

SAME AS ABOVE WITH 4 TURN $\frac{1}{8}$ " DIA. COIL BETWEEN 6111 PLATE AND TUNED CKT.

400 85 402.5 - 35 DB

SAME AS ABOVE WITH A 1 μ f CAP. ADDED TO GROUND FROM 6111 PLATE.

400 85 402.5 - 38 DB

SAME AS ABOVE WITH THE ONE TURN IND. REPLACED WITH A STRAIGHT BUSS WIRE.

400 85 402.5 - 50 DB

NOTE: BY DIPPING SIGNAL ON RESPONSE THE RESPONSE WAS DOWN - 62 DB.

OSC. SAME AS ABOVE.

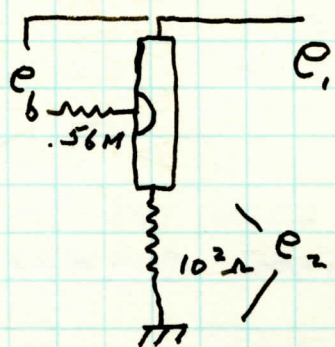
309.8 76 310.5 - 62 DB

OSC SAME AS PAGE 30
FREQ. SEN. RESPONSES

260 62 NONE

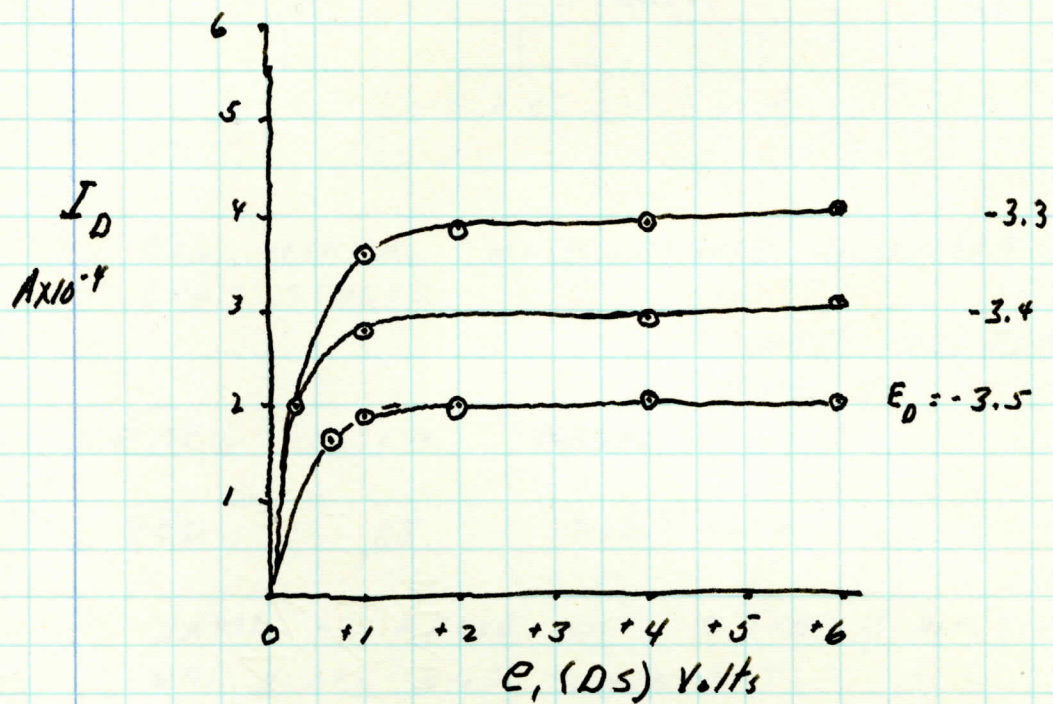
WITH STRAIGHT BUSS WIRE REPLACED WITH
ONE TURN IND.

260 65 NONE



Device: Mot. plastic

$$I = \frac{e}{r} = \frac{10^{-2}}{10^2 \Omega} = 10^{-4} A$$



Amplifier design $\bar{c}$ FET's

Seems safe to assume $H_i Z_{in}$

Gain at VLF and temp var. are unknown -

$$E = IR$$

$$\frac{1}{.2 \times} = 500 \mu A$$

$$Z_{out} = \frac{\Delta \theta_o}{\Delta \theta_i} = \frac{1}{10^{-5}} = 10^5 \Omega$$

$$G_m = \frac{\Delta i_o}{\Delta e_g} = \frac{.9 \times 10^{-4}}{10^{-1}} = .9 \times 10^{-3} = 900 \mu mho$$

$I_D = 2 \times 10^{-4}$
 $E_{D_s} = 1.2 V$
 $E_g = -3.5$

$E_{D_s} = 2.0$
 $E_g = -3.5 V$

For $A = 10$

$$A = g_m R_L$$

$$R_L = \frac{10}{9 \times 10^{-4}} \approx 1.1 \times 10^4 \Omega$$

$$E_{R_L} = 10^4 \times 10^{-4} = 1. V$$

Although FET's with sharper cut off, lower pinch off & possibly higher g_m 's may be found the requirement for opposite polarity supply for bias, reasonably high load resistors and accompanying large drop, and degeneration for temp. stability all are incompatible $\bar{c}$ a low voltage low current ckt. Insulated gate FET's may be operated at 0 or + biases $\bar{c}$ + supplies but large supplies and currents are required. Future developments may make these units more attractive transistors $\bar{c}$ high β at low I_c have reasonably high Z_{in} now - with $\beta = 200$ an emitter of $\frac{10^6}{2 \times 10^2} = .5 \times 10^4 = 5K$ for 1 meg. in is required. Looking at temp. in

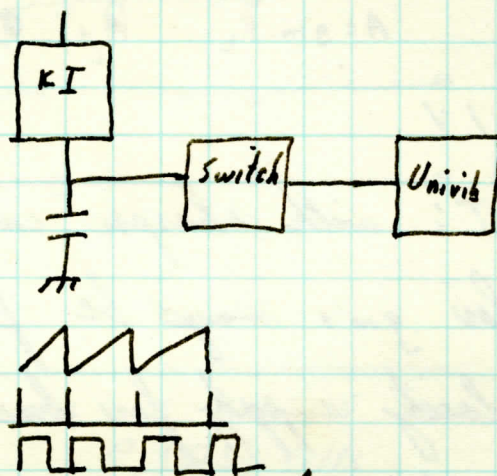
$$100 \mu A / 100^\circ$$

$$\frac{100}{30} = 3 \mu A / ^\circ C$$

$$30 \mu A / V$$

$$.3 \mu A / mV$$

a MOS FET, the var. is $3 \mu\text{A}/^\circ\text{C}$ at low voltages (null is 6.V) and gm. is $.3 \mu\text{A}/\text{mV}$ at some point. The present SCO sets limits on the amp. and should be approached first. In the crystal mode some form of switching will be required so the linear pulse rate with a pulse stretcher should be considered.



A constant ^{pulse} bandwidth will lend itself to additional discrimination.

$X_{ta}/R_{err} + X_{mtr.}$

$$\begin{array}{r} X_1 - 11\overset{9}{8}.15 \\ 108.7 \\ \hline 10.75 \end{array}$$

Freq	300	600	1200	2400	48	9.6
80	0	.82	.4			
85	0	1.3	1.1			
95	.98					
105	1.9	limits	limit			
115	1.89	@	93db			
90	.220	90db		90db		
75		.002				
		Thresh 77	Thr-78	Thresh 78		