

Construction + Operation
of

Mod 2 B Radar Optic

FE1

Developed by

W^m Thornton

mm

This F.C.I. system was ~~des~~
designed and developed at A.B.G.C.
as a unit which ~~is~~ could be built,
operated and
maintained by field ~~to~~ operational
units with suitable shop facilities.

It is a new and simplified design
of a ^{radar optic} scoring system developed here.
~~It works~~ A prototype was built
and ~~operated~~ ~~to~~ run down
as many bugs as possible as well as
to determine operating procedures. Ideas to
further simplify this unit have been
constantly appearing up ^{there} to the time of
of writing and they will undoubtedly
continue to do so. The unit appears to
be relatively bug free however for the
total maintenance ~~to~~ during some 12 or

2
15 missions has been the replacement
of 1 fuse which was underated.

All items used ^{except one} are stock and are
listed. The one exception is a camera
since the Air Force has no ^{suitable} motor
driven 35 mm camera available. ~~The~~
Camera used is a Model 4 c mfg
and sold by Flight Research Corp.,
Richmond Va. This camera is almost
ideal for the job and little difficulty should
be experienced ^{obtaining} ~~obtained~~ them. Any motor
driven 35 mm camera with frame
rates of 20 to 50 per second would
be suitable with slight modifications to
the ^{A scope} combining system. At present, work
is under way ^{here} in the Photo Optic

Lab to fit the A-T to this installation.

Theory of operation of this ~~form~~ method of scoring ~~run~~, simplified, runs as follows. A motion picture record is made of ~~the~~ rocket's path past the target by a camera in a chase plane flying through a firing run in formation with ~~the~~ firing aircraft. Concurrently with ~~the~~ strike camera record a record is made of a radar A scope presentation on which is displayed both rockets and target's ~~range~~ from relative range. When ~~the~~ range of pattern centroid is coincident with target range ~~a~~^a corresponding photograph is taken from the strike record. Miss distance is obtained from this film frame of film by comparing miss distance

of centroid to target length.

In this ~~Mod. 26 scoring~~
F.F.I. functions of strike camera and
scope camera are combined to eliminate
difficulties of synchronizing camera, assessment
problems and others. A modified 4" Baltar
lens is removed from its lens barrel and
screwed into ~~the~~ an adapter ~~in the~~

Drawings # 4 + 7 ~~to~~ These
lens are focussed individually at the factory so
it will ~~not~~ be necessary to refocus them
on the modified barrel by screwing ~~the~~ lens
proper onto ^{modified} barrel in ~~a~~ correct position
and pinning it there. This can be accomplished
on an optical bench or more simply on a
camera with a ^{bore sight} bore sight tool. The 4" lens
images ~~the~~ strike information on the film while
a 2" lens set in the adapter images through

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~~[Drawing 4.5]~~

a mirror onto one edge of frame aperture
A scope information. In order to place
this cathode ray tube in a practical practical
position it was necessary to use a
mirror mounted on the camera (Drawing ^{4.5})

~~This lens leaves something to be desired in
speed as it is only F 4.5 max and for
this reason the shutter opening on this ^{image} portion
of ~~the~~ is increased (Drawing, 8)~~

~~It is absolutely mandatory to use a
31 P 11 tube for the much higher actinic
value of its phosphor. At these writing speeds
light from a green phosphor P-1 will not
produce an acceptable trace. Class L film
is ^{also} used to gain a slight ^{speed} advantage.~~

See drawing ~~(4.6)~~ for mounting
detail of cathode ray tube. Power for
this tube is from a high voltage supply used
in pilot's presentation of ~~F-36-D~~ F 94 C

To ~~pro~~ provide necessary voltages for an 'A' presentation on the 3SP-11 a sweep and video circuit simple to the point of crudity is used. It ~~fit~~ is entirely adequate however. ~~For~~ All power plus trigger and video pulses are obtained from a G-30. This unit is constructed on an ~~and~~ aluminum chassis ^{Drawing 3} which fits the same type shock mount as ~~the~~ voltage regulator of the G-30. (Fig 4 t/8) Video amplifier is a straight R.C. coupled pentode receiving video information from the video jack ^{G-30} on range computer and power supply. ~~R₂₀ is~~ R₂₀ is kept ^{low} small to maintain time rise of ~~the~~ pulses. It first appeared that some form of peaking network would be ~~neccos~~ necessary to keep ~~the~~ out put ckt 'fast' enough and yet with a reasonable gain however this ^{is} was

not necessary if all leads are kept short and good high frequency practice is followed in construction. ~~It~~

A negative ^{trigger} pulse from ~~the mo~~ from the G-30 R.T. unit initiates sweep and unblanking functions. ^{Drawings 14 & 15} This trigger is coupled thru ^a diode V_1^* to ~~the~~ the normally non-conducting plate of a univibrator - ~~The~~ Current is drawn by this trigger causing ~~the~~ conduction in this ~~two~~ triode while the other is cut off. This state remains until enough charge has leaked off C_3 and C_4 for the circuit to return to its normal state. Output of this circuit is a large negative pulse which may be varied in duration from ~~one~~ to 3 to 15 microseconds.

This negative pulse gates the sweep and intensifier ~~ckt circuits~~ through C_5 and R_9 .
* This tube has later been replaced by two 1N34A diodes in series.

To keep screen burning and other undesirable effects down, ~~the~~ beam of Cathode ~~ray~~ tube beam is turned on only during sweeps.

A negative gate is applied to $\frac{1}{2}$ of

V_3 which is conducting heavily causing the tube to cut off ~~with~~ ^{Diagrams 14+16} A. An almost square pulse is then applied to the grid of V_6 (31P11) ~~turning~~ allowing beam current to flow for pulse duration.

To generate necessary sawtooth voltages for sweeps a negative gate is applied to clamp tube V_3 cutting it off and allowing plate voltage to rise ^{Diagrams 15+17} A. This rising grid voltage is applied ~~to~~ directly to the grid of $\frac{1}{2}$ of V_4 - This tube triode has a large amount of feedback from plate ^{to grid through $C_6 + R_{14}$} ~~of high~~ ~~variational impedance~~. The resulting linearly increasing voltage is ~~fed~~ coupled to a horizontal deflection plate of 31P V_6 .

thru C_{16} and a portion is applied to ~~the~~
grid of the other triode of V_4 which is a
paraphase inverter. This tube inverts the
sawtooth which is now applied to the other
pt deflection plate of V_6 thru C_{16} -

~~The~~ Circuitry is simple and straightforward.
There is room for improvement in layout
especially high voltage components. To
set this circuit up a scope ~~such as~~ with
excellent high frequency response ^{must} ~~should~~ be
used. ~~Couple~~ A 5.5 S. 239 should be
adequate. Through a high impedance
probe ~~to~~ couple the plate of V_1 to the scope
and apply a negative trigger of about 25
volts to V_{302} . This trigger can ~~should~~
be the trigger pulse of a $6-30$ but may be
synthetic. Adjust R_7 until the pulse ~~form~~
is 'locked in' with the trigger. This can be
determined by removing the trigger which should
~~also remove~~ ^{stop the} ~~the~~ pulse. Too high a setting

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of this control will result in inability to trigger the circuit while too low a setting will cause the circuit to run free without triggering. Correct setting is ^{1/2 way} between these points.

Q. Next move the probe to ^{pin 2} plate of V_3 where a ^{square} positive ^{pulse} will appear. Width of this pulse controls width of range displayed on the A scope. Scale factor is 490' / microsec. G_4 should be adjusted until desired range is obtained. Settings of 5 to 7 micro seconds are normal.

~~Next~~ Display positive sweep on the scope by going ~~to~~ pin 5 of V_4 . C_6 must be adjusted for proper sweep rate. Too fast a rate will result in a rise to a sawtooth rising to a maximum and becoming flat for the remainder of the pulse while too slow a rate will mean a decreased amplitude. Correct setting is ^{just beyond the} ~~go between the points~~ where flatness ends and where decreased amplitude is noticeable.

With a little experience all of these adjustments may be made by merely watching A scope presentation.

The G-30 is strictly stock with only tubes V

being removed to decrease power drain. T.O.'s ^{for bench checks} apply completely except to the range and other circuits disabled by removal of tubes.

~~There is one other exception when the~~

Cable diagrams for this installation are given in Diag # [12 & 13]

Primary power wiring in plane and tank are given ~~in~~ # [10]

In order to eliminate any possibility of ^{with firing aircraft system} interference ~~and~~ primary of the magnetron A.C. supply is connected only ~~during~~ a few seconds before and during firing.

Power for ~~the~~ scope power supply

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is taken from any convenient point
on the 115 V 400 N supply through
a 1 amp fuse. This is not shown
on these diagrams. Ship's wiring is
given in Drawg. 11. A single point push
to make ~~not~~ switch is placed in the
tank for convenience in preflight. This
operates camera and radar.

To prevent ^{an} overloads on G-30 component
since additional filament and plate power
is drawn from it ^{tubes in the range} ~~computer section~~ ^{# V-} which are not used in this circuit ^{should be removed}
~~are removed~~. Other than this it is unmodified.
Set A.G.C. threshold until AGC volt is
-1. If gain is insufficient this may be
reduced. Do ~~Not~~ Not connect the trigger
cable from R.I. unit to ~~the~~ Range Computer
as this will operate a ducking circuit
that obscures the ~~for~~ first portion of the
trace.

Construction and mounting details are
given in Drawg. # 1, 2, 3, 4, 5 & 6. These are
detailed enough to be self explanatory.
P This report was ^{hurriedly} assembled and
there are undoubtedly ~~some~~ blank areas
however we have readily available
any additional information necessary.

26 as a method suitable for field use
proves ~~the~~ feasibility of this system, a
~~separate~~ complete system including radar, cameras,
and A scopes. ^{was assembled} The R.T. unit of a G-30
was housed in a 120 gal M-116 napalm
tank along with an A scope presentation
which was photographed by a camera ^{35 mm}
whose shutter openings were synchronized
with those of another 35 mm ^{strike} camera
~~which served as a strike camera,~~
equipped with a 4" lens. This unit was
~~and~~ suspended from an B6 F.
hurriedly assembled and without preliminary
tests taken to Yuma A.T.B. where
~~intensive rocket~~ a large number of
firings were being made. During the week
~~there~~ ³ successful firings were ~~made~~ ^{chased by this B6} with
all 3 being successfully recorded. ~~the~~ ~~this~~
This instrumentation in spite of its hurried
design and construction and unnecessary complexity
~~performed~~ required no maintenance.

~~Results were all Results were extremely
 gratifying. Several hits were recorded
 which thus affording a check against
 instrumentation accuracy which proved to
 be excellent. This was the first instance
 of a firing error indicator functioning
 successfully in the field. Several conferences
 were held with people or members of
 Air Defence and Training Commands as to
 the most useful satisfactory configuration
 of this system and it was decided that a
 chase plane equipped with this F.C.I. offered
 more advantages ~~primarily~~ than any others.~~

^{simple}
 A unit was then designed using
 with one exception, a stock A.F. items which is simple enough
 to be reproduced by any well Air Force
 installation ^{equipped} with machine shops and facilities

M-26

This scoring method is extremely versatile requiring ~~on a~~ basically only two sources of data, radar video information and photographic data from a strike cameras.

We have built a series of these ~~see~~ Radar-Optic ~~see~~ F.E.I.s ~~here~~ using various configurations. They have fallen into roughly two ~~for~~ ^{units} classes. ~~It~~ systems mounted on the firing craft and using system's radar for video and those mounted on a chase plane with its own radar. The system ~~describes~~

~~The sys~~

~~described~~ described in the following is the Model 26 which was designed for field use. It consists of an unmodified G-30 radar feeding a 4 tube sweep and video chassis ~~which~~ whose output is

M-2.6

an 'A' presentation on a 3SP11
cathode ray tube. A modified lens combines
the image along one edge of the 35 mm
film ~~along~~ with strike ~~on~~ photographs. A
40 fps frames per second camera
is used. Housing for the unit is ~~an~~ ^{an}
M-116 napalm tank with necessary
changes ~~to~~. Weight is approximately
125 pound and drag is only slightly
higher than a normal tank. The
chase plane flies a fairly tight formation
with firing craft and during the last
~~the seconds~~ few second ~~last~~ of a firing
run radar* and camera are turned on
for ten or 15 seconds.

* ~~High~~ Voltage is ~~only~~ applied to the magnetron ^{only} during
~~this~~ ⁹ period to eliminate possibility of interference

for maintaining an 'E' system. A prototype of the unit was assembled and tested here and will be given to Yamp for further tests. This Complete ^{details of} construction and operation of this ^{FEL} unit are given in the attached appendix.

Since the concept of tracking ~~rock~~ missiles with pulsed radar is relatively new and ~~off~~ opens a realm of possibilities in the missile field in general its specific application ^{for E system scoring} to as a practical F.C.I. ~~system~~ will be described in detail ^{some} ~~TP~~ Restating the problem of photographic scoring: Ranging of ~~missiles from missiles~~ miss of rockets miss by motion picture photography is easily accomplished by stadiametric technique if ~~the correct~~ and only if a rocket is in or near a ^{perpendicular} plane normal to the longitudinal axis of the strike camera is a plane ~~through~~ through the target

insert photograph on M2 b

parallel to the camera's film plane. Accuracy

First order accuracies are determined solely by the ~~correctness~~ errors in detecting the cutting of target plane by ~~the~~ rockets and relation of this to the strike camera film. A positional error thus become a function of time errors as the target is in continuous ~~on~~ linear motion.

An example will illustrate. Assume that the ^a ~~single~~ strike rocket ~~or centroid of a pattern~~ crosses ~~the~~ a target plane ^{where} at some given time missing the target aim point by ~~50 ft~~ ^{50 ft} ~~left~~ ^{lead} in azimuth. Suppose that a photograph

is taken ~~some~~ $\frac{1}{20}$ of a second later and miss distance is assessed ~~data is taken~~ from this photograph. Errors

in azimuth will now vary directly as the speed of ~~it~~ target speed. Elevation errors are negligible since ^{vertical} target velocity is zero and ^{relative to the firing aircraft} vertical rocket velocity ^{is} arises only from gravity acceleration

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which is on the order of $\frac{70 \text{ ft}}{70 \text{ sec}}$ at this point. Errors in azimuth will now vary directly as target speed. ~~In this~~ In this case the ~~with~~ target will have the missile will appear to have ~~to~~ passed ~~it~~ closer to the target by ~~the~~ distance ~~the~~ ^{of} to target travel in $\frac{1}{20}$ sec. With a target speed of 300 ft/sec this error in azimuth would be $15'$ against an elevation error of $3.5'$. It is obvious that the relation

Error in ~~distance~~ assessing target velocity $\left(\frac{\text{ft}}{\text{sec}} \right)$
miss distance in azimuth (ft) $\times$ error in determining time of crossing rocket plane (sec)

holds for this specific case.

^{much smaller} Other errors are present in ranging technique but this time function error predominates.

This of course leads to a ~~more~~ ^{another} fundamental problem. Since rockets are fired during a relatively long period of

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* should be footnoted *
time (approximately 1.25 sec for ^m890, ^{.084 sec.} ~~#~~ for 860

and .168 sec for ~~EF-94~~ for full salvoes) ~~so~~
the rocket pairs must be followed separately
and the time of crossing crossover time ~~to~~
recorded ~~under~~ for each pair or one rocket
must be chosen and the time of only this
pair's crossover be recorded. The first procedure
is ~~for~~ necessary for extremely accurate work
in engineering tests. For evaluation of system
accuracy it is enough to know where the so
called strike rocket or pattern centroid ^{goes} for
it is this rocket which is theoretically designed
to hit target center target aim point. Since
neither missiles or ~~sgt~~ fire control system
is perfect it is necessary to add rockets
~~be~~ fired before and after the strike rockets
to bring kill probability to a reasonable
figure. It is ~~for~~ the centroid which is
scored with the system being described

X

32 by interpolation

although it is possible to score other rockets.
~~Since~~ ~~Since time~~ ~~Q~~ Radar ~~to~~ without

sets used to determine range coincidence
~~Set~~ is ~~any~~ ~~Q~~ ~~AV~~ ~~APG-30~~, an
airborne, ^{low power,} X band set with 5 KW peak ~~p~~
commonly used for range data on A series
sights. It would be desirable to have a
set with more power or ~~at least~~ an antenna
of smaller beam angle but this is more
than offset by such factors as small ~~size~~,
light weight, simplicity and ease of maintenance.

Range information is displayed on a 3"
scope in an 'A' presentation. In this
presentation the ^{coincident with transmitter output pulse} beam is started ^{scope} at one
edge of the tube and is swept linearly
across the face ^{along X axis} ~~of the tube~~ If Return pulse
information is displayed along ~~the~~ X axis the

resulting ~~path trace~~ in ~~range~~ scale giving
~~range~~ on which ~~range of objects~~ distance
 of objects from the set may be determined.

~~Absolute range is~~ Relative not absolute range
 is of primary interest here.

Since extremely short ranges are ~~used~~
~~of~~ ~~not~~ necessary here some complications
 arise since the sets are designed for much
 longer ranges. Radar range factor is

approximately 490 ~~per~~ ~~micro sec.~~ ~~with~~
 thus the .4 ~~microsec~~ pulse of ~~a~~ ^{this}
 G-30 covers 196 feet in space. ~~Objects~~

closer together than this cannot be separated
 on ~~a~~ a presentation. Ideally ~~the~~ pulse length

would approach zero with position of
^{each scanned}
~~an~~ object appearing as a single narrow line.

Unfortunately practical limitations prevent this.

~~so that~~ ~~Rockets~~ A salvo of rockets
 appears as a single ~~pulse~~ lengthened pulse

and the target as another relatively wide pulse.

After a little experience ~~pulse~~ ^{time of}
^{for the centroid} ^{by inspection}
 crossover's can be determined to within
 one frame of film run at 40 frames per
 sec even though ~~the~~ pulse width occupies
 a relatively large amount of trace width.

~~Once correct~~ At forty frames per second
^{azimuth} ^{time}
 the maximum error is less than $\frac{1}{40}$ second ~~X~~
 tow speed. At present speeds this is on the
 of 7 feet. Elevation error ~~is~~ is negligible.

Once ~~the~~ ^{instantly} ~~moment~~ of crossover of the
^{found it is} centroid is ~~only~~ ^{only} necessary to ~~choose~~ ^{select} the
~~centroid~~ and of the pattern from strike
 photographs and determine magnitude of
 miss ~~from~~ stadiometrically. For use with
 present targets a slide projector would be
 desirable but not necessary. Experience here
 has shown that pattern centroid is extremely
 close to the center of a circle which encloses

all but obviously wild rockets. Choosing this point becomes simple after ~~comparing~~ observing several strike films. One this point is chosen magnitude of miss is determined by comparison of ~~appears~~ it is only necessary to compare its distance from aim point * with target length to determine image miss distance to image distance of centroid from magnitude of miss. aim point * to image distance of target,

~~Advan~~ This system approximates has much to recommend it. Indeed it is difficult to conceive of ~~of~~ ^{other} any system with the advantages of no target limitations, ~~at~~ ~~very~~ simple data reduction, and a ~~record~~ photographic record of the firing passes realistic enough to evaluate offer incentive to a pilot to study his performance. It is to accurately evaluate a pass with any form of FEL it is necessary to have a record of pilot's performance to determine errors introduced from steering.

~~Advan~~ As mentioned before ~~the app~~ * aim point on a non reflective banner with corner reflectors attached is of course the reflectors. It will vary with reflective targets.

the use of radar to obtain range data from missiles has many applications. It should be an extremely valuable tool in ballistic studies of velocity, acceleration, and pair dispersion. As an F.O.D. system its value is obvious. Many possibilities exist for its immediate utilization. ~~Most~~ ~~or~~ ~~readily~~ ~~available~~ There is no reason why the Model 26 F.O.D. as described in the appendix should not be immediately reproduced for use at bases where firing programs are being conducted. At present it seems impractical to equip individual fighters with this system even though it would involve only a simple 'black box' and a camera. ~~It~~ Such an installation would be far simpler than the Radar equipment which is presently being scheduled for installation. It would be of vastly more use. ~~A~~ Value of

an F.C.I. system needs no ^{further} justification.

~~The development of this system should have far reaching effects ^{on} to targets. Now instead of having to use banners as a crude attempt at scoring, ~~it~~ only function ^{of a target} need be provision of a radar target with realistic performance. A logical target configuration would be a radar reflector enclosed in a streamlined structure offering small drag. Once drag is reduced to a low figure it is possible to reduce cable size weight and drag as well as reduce tow reels ~~to~~ size weight and complexity. With this reduction in size weight and drag the next logical ~~step~~ step is use of fighter craft ~~to~~ to obtain realistic performance. ~~That~~ Work has been done toward developing small low drag, ^{radar reflective} targets~~

by a least two companies one of targets ^{whose}
 has the added feature of fragility
 which should be extremely attractive for
 training use. A prototype of a high speed
 target was ^{recently} constructed ^{here} and preliminary tests of it
 are under way. ~~A~~ Drag of such targets
 are ~~in the~~ approximately 50 lbs at
 300 knots T.A.S. Weight while weight is
 20 lbs. or less. Radar reflector area is
 equivalent to a ^{3' diameter} conventional round reflector.
~~If~~ there are ^{nylon} commercially available fishing
 lines which have adequate strength to tow
 these targets. With small cable reel sizes
 can be cut to reasonable figures. It
 is a relatively minor problem to design
 a reel such that it could be carried under
 the wing of a fighter in a nacelle which

could also partially house the target
 for takeoff - ~~Probably most practical~~
 of all would be a ~~system~~ target and
 small reel which could be attached
 to a conventional ~~war~~ bomb or tank
 rack ^{of a fighter} ~~and~~ Once airborne the target could
 be released and after completion of
 mission both target and cable be
 detached from aircraft. This is an
 entirely feasible system even from an
 economic standpoint since cable and
 target should cost less than \$50. At present
 a marquisette target costs and reflector
 costs almost \$300. Seven of the smaller
 targets ^{discarded after every mission} would provide much longer time
 in the air than a single banner. ~~and at~~
 These targets would ~~also~~ provide performance
 performance which banners never can.

If cost of maintenance of a present bomber type tow plane ~~were~~ are compared to ^{those of} a fighter using small targets, target price becomes insignificant. Fighter type tow craft would provide ~~squad~~ individual squadron with presently lacking tow facilities. There are many squadrons which if tow facilities were provided could carry out on firing programs rather than indirectly ~~show~~ 'shadow boxing' which is the extent what ~~at~~ the present training amounts to.

~~The radar~~ The radar optic scoring system described is a presently available ~~not~~ for immediate application to ~~the~~ scoring of 'E' systems equipped ^{and presently unique} interceptors. New ^{and presently unique} methods are involved but ~~it~~ but this is necessary if we are to

close the ten year lag that presently exists in
town target facilities. ~~Even though this system~~
~~is at presently the importance of a~~
~~satisfactory~~