

Measurement of mass under zero G conditions -
Most of the methods proposed so far depend
upon 1) making the mass part of an oscillatory
system by the addition of a compliance and
measuring periods: $\frac{1}{T} \approx \frac{1}{\sqrt{2\pi MC}}$

2) spinning it placing the mass in a circular
orbit and measuring the force developed.

$$F = \frac{1}{2} \frac{mV^2}{R}$$

3)

2. The difficulties in method 1) differ in lack of complete coupling of all parts of a man's body.

2) variations in distribution of mass as a function of length during measurement

Reference to 2.1 -

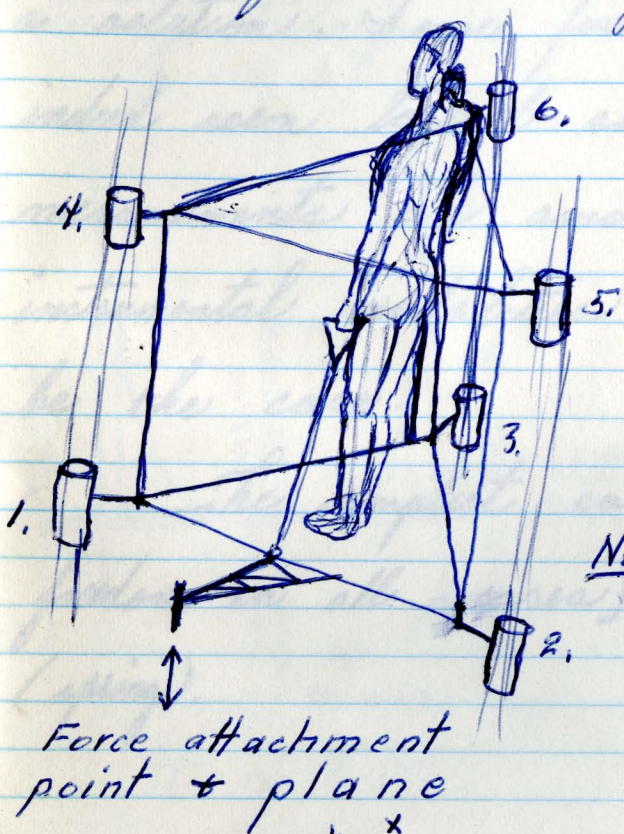
Coermans et al. Luftfahrtforsch. V 3 P 111
1938 - see also V-IV A-6636 668 Medical Physics
show that deviation from linearity ($m\omega$) is negligible
below 3 CPS when sitting in abdominal restraints.

Fig. 1 { $\theta = \frac{y}{r}$ + $r = \frac{y}{\theta}$

R = Force applied y = resulting Force in Y plane

$1^\circ = .9998$ $2^\circ 30' = .999$ (.1%)

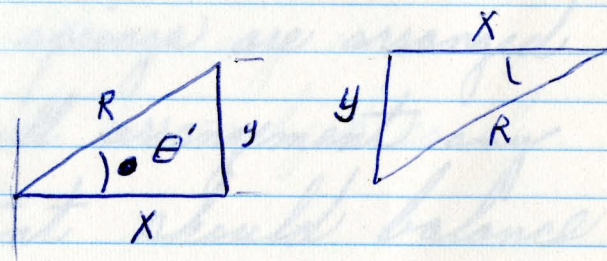
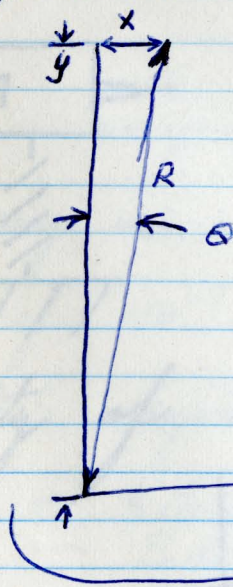
It would seem hopeless to attempt to solve the problem of restraining the mass to a single degree of freedom. In addition a reduction in the motion of individual body components may be effected -



1-6 are low friction bearings to restrain the platform to a single degree of freedom - (Vertical)

Not to SCALE or Proportion

Variations of force as a function of variation from a given plane



$$R = R - y$$

$$R = \frac{\tan \theta}{x}$$

Fig. 1 { $\cos \theta = \frac{y}{R}$ + $y = \frac{R \cos \theta}{\cos \theta}$

R = Force applied

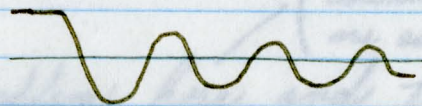
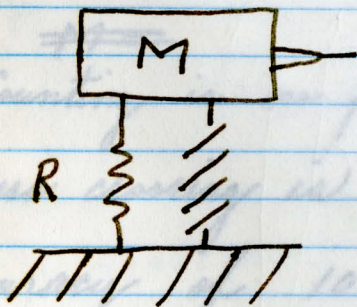
y = resulting Force in Y plane

R

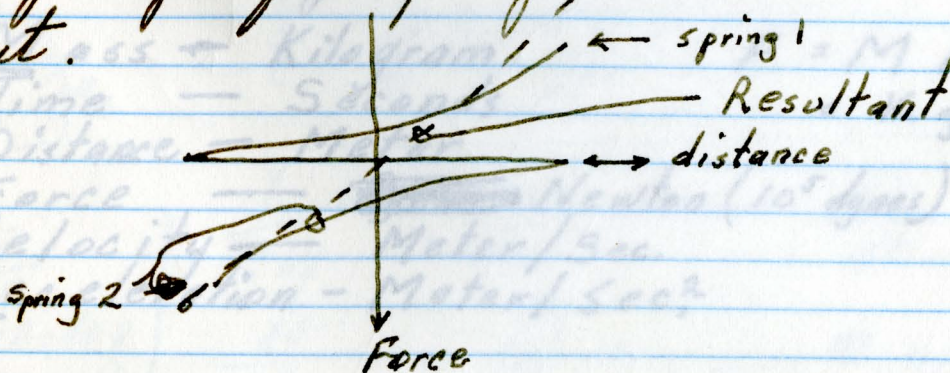
$$1^\circ = .9998 \quad 2^\circ 30' = .999 \quad (.1\%)$$

At first glance an analog of capacitor R.C.R. circuit measurements might seem most logical for a solution. Some form of frequency determination would indeed seem logical since time & frequency measurements are among our most accurate instrumental modalities. This however may not be the case.

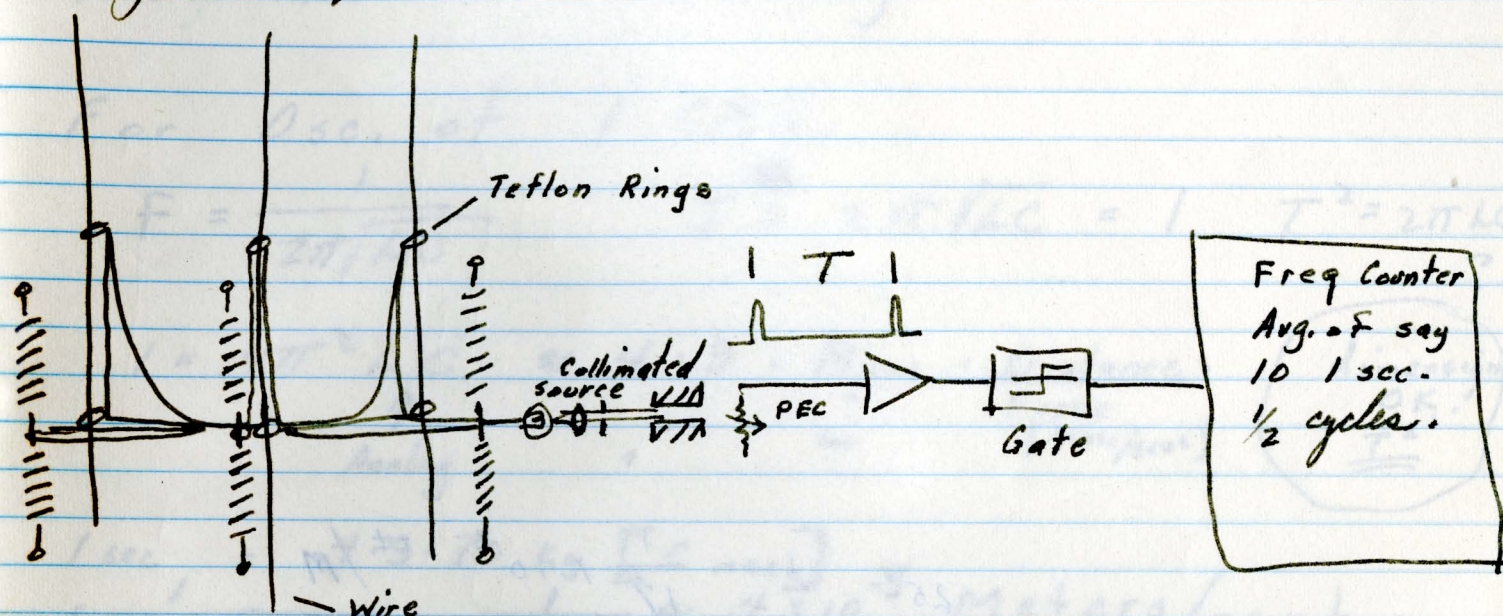
The simplest case is (assuming 1 degree of freedom in all cases) addition of a compliance (spring).



If the springs are arranged in a push-pull arrangement any irregularity of spring constant should balance out.



A displacement could be applied and the frequency of the resultant damped oscillation measured by timing techniques.



$$T \sim \sqrt{M}$$

Counting is no problem here and the detection of zero crossing is a mechanical problem - say an accuracy of 10^{-3} ins. and should be realized easily. (counting accuracies of 5×10^{-5} are easily available)

In M K S system -

Mass - Kilogram

Time - Seconds

Distance - Meter

Force - ~~Dynes~~ Newton (10^5 dynes)

Velocity - Meter/Sec.

Acceleration - Meter/Sec.²

$$F = M A$$

$$= \text{Kg.} \cdot \text{Meter/Sec}^2$$

Equivalents:

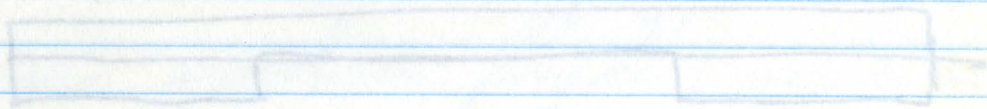
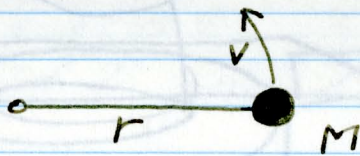
$$1 \text{ Newton} = 10^5 \text{ Dynes} = 3.60 \text{ oz}$$

$$1 \text{ #} = 4.448 \text{ Newtons}$$

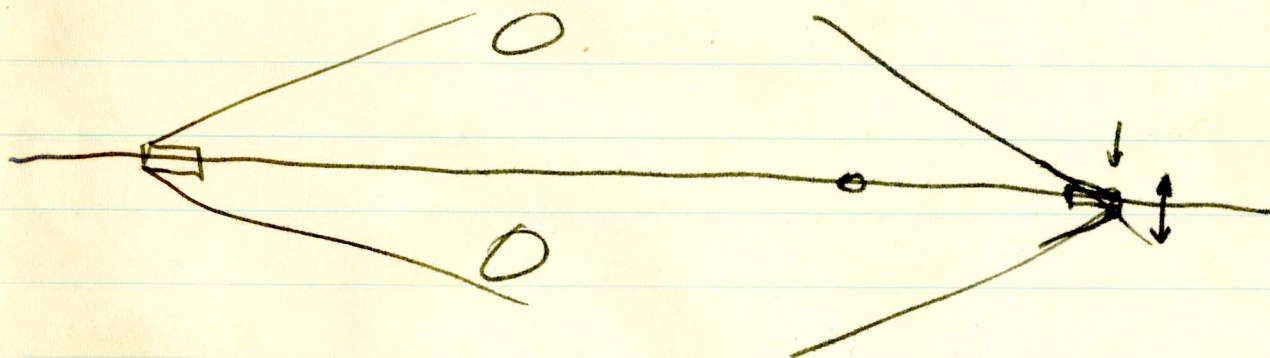
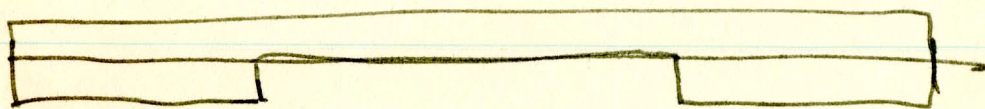
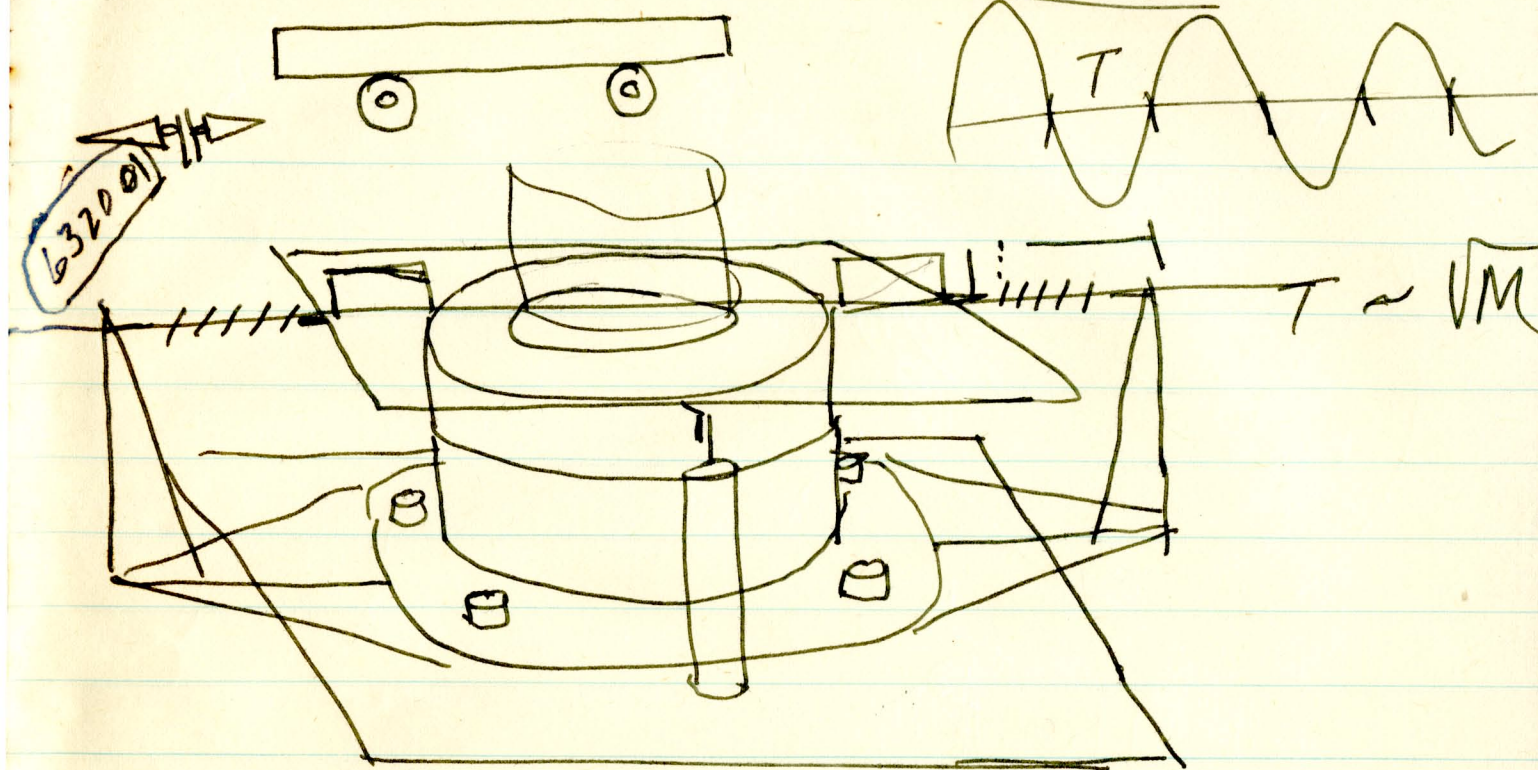
$$1 \text{ gm. wt.} = 980 \text{ dynes}$$

(Col. Carter)

Effects of a rotating wt.

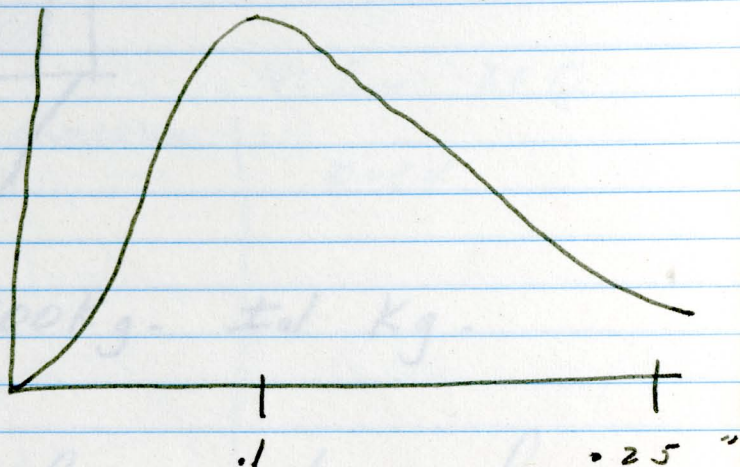


(Col. Carter)

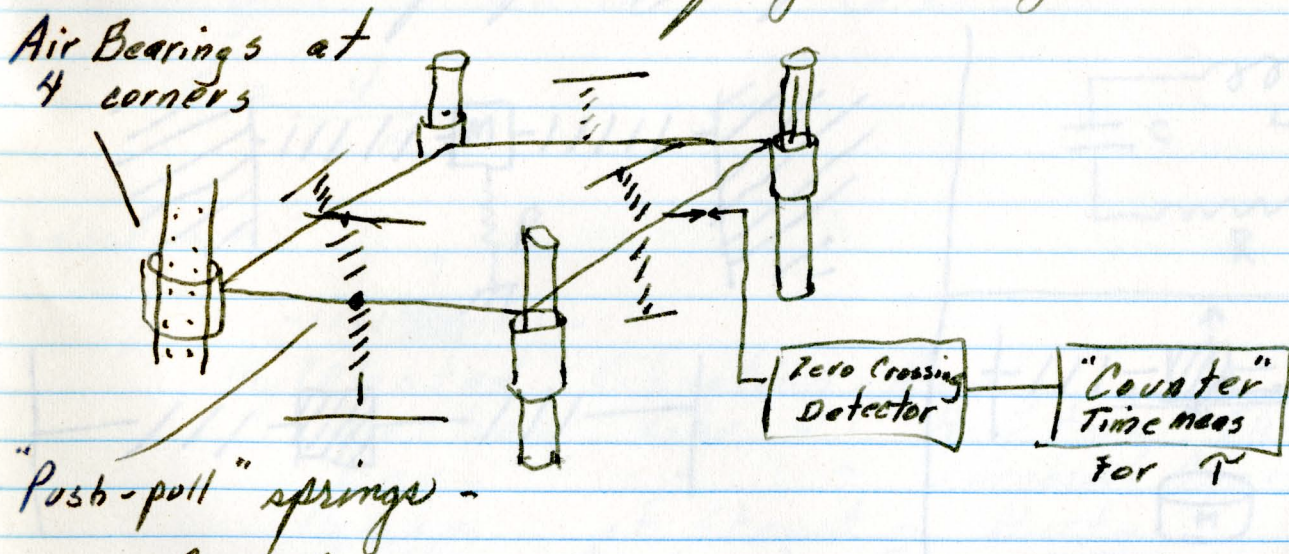


25 Aug. '65

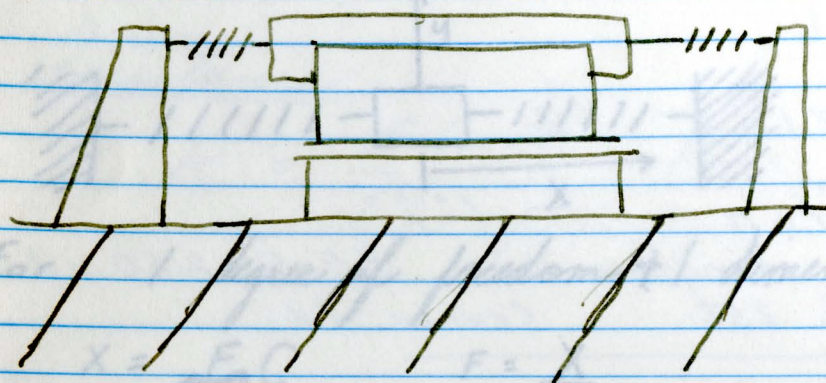
Called Mechanical Technology Inc.
518 - 785 - 0922 Mr. Springstead about
their Optical Dist. Sensors which is a reflectance
device. I have the following
transfer curve but
might be modified to yield
 $\frac{1}{2}$ mil res. at
 $\frac{1}{4}$ " working dist. 2v.
Has 2 mv. noise, $\frac{1}{4}$ " probe.
std. 1000 + 2 wks. deliv.
Still send quote +
max. performance -



He will do a simple exploratory model
using the air bearing as soon as possible.
Can see no reason why the scheme below
will not work in flight (weightless)



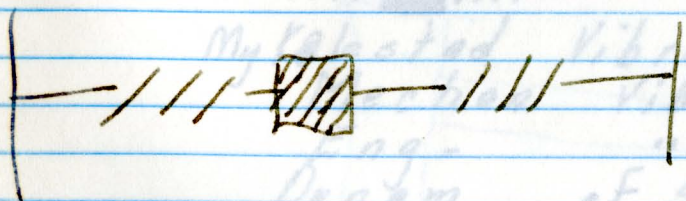
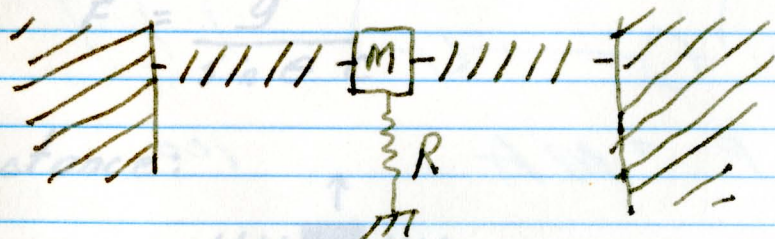
Such an arrangement could be incorporated
into a normal seat which would be
locked into posn. when not in use.



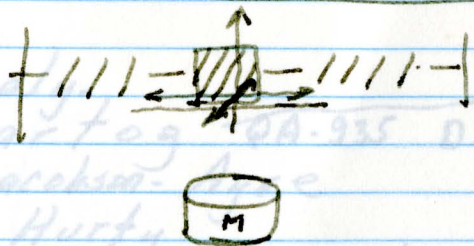
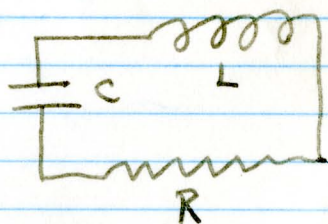
Range of Mass - 50-100Kg - ± 1 Kg.

Accuracy 0.1%

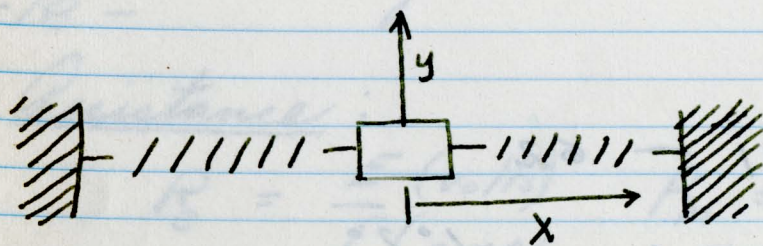
Method: determination of period $\bar{t}$ the unknown mass made a portion of ~~the~~ an oscillating system at a nominal frequency of 1 C.P.S.



Quigly - Hughes



→ Earl Bell ←



For 1 degree of freedom + 1 dimension:

$$X = FC$$

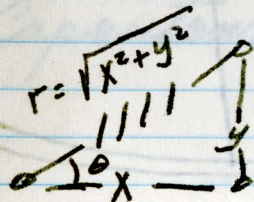
$$F = \frac{X}{C}$$

$$F = \dot{X} R$$

V: Force $X \dot{=} Q$

$$Q = CV$$

For 2 degrees: dimensions:
Capacitance:



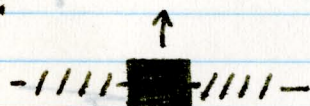
$$\sin \theta = \frac{y}{r}$$

$$\cos \theta = \frac{x}{r}$$

$$y = F \sin \theta C$$

$$F = \frac{y}{\sin \theta C}$$

Inductance:



My Kalesad Vibration - Analy.

Mechan Vibr. - Hartog QA-935 D3

Eng - " - Jacobson-Ayoe

Dynam of Struct - Hurty

Vibr. Prob. in Eng. - Pambleschenko

RC-1100 S-72

Coernmann

QA-871 C-72

QA 871 KB2

RC-1125 H-27

TA-355 M74

TA-355 H27

QA-935 T4

Nortronics -
213 · 772 · 2321

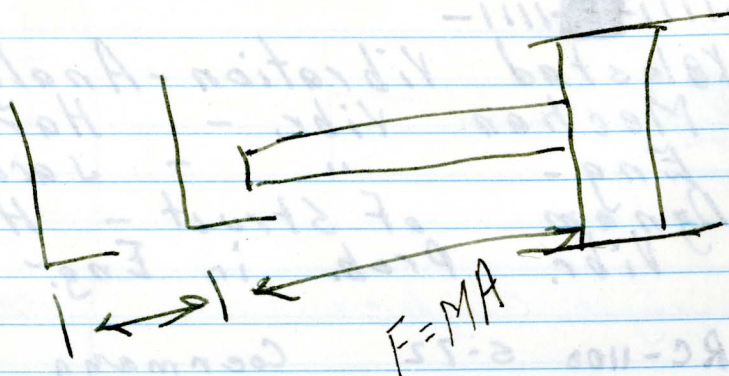
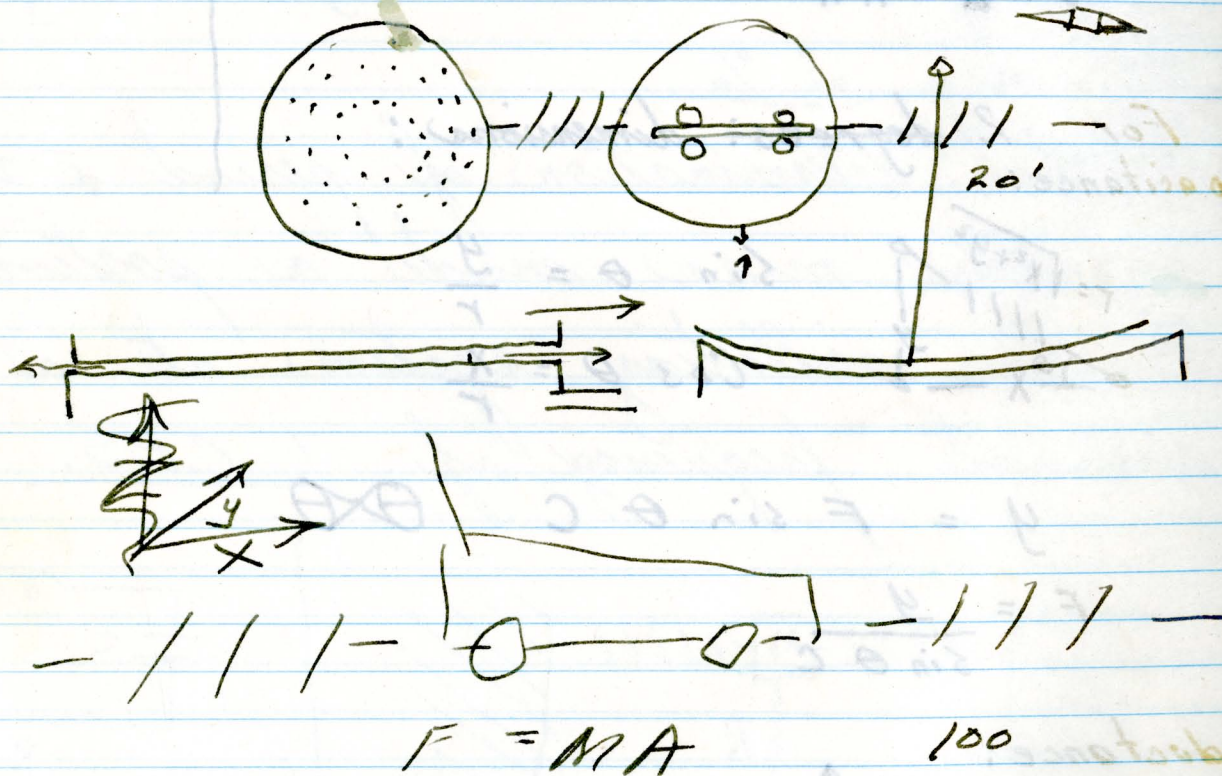
Hughes -
213 · 391 · 0711 - 62

Paul Crafton · 1° 2°

Geo. Washington Univ. FE 80250 · 202
Ext. 258 Cronin · 721

Dept. Mech.

Sgt.



From Olson, Dynamical Analogies:

P-18 -

Resistance:

$$R_e = \frac{E \text{ (volts)}}{I \text{ (amps)}}$$

$$R_m = \frac{F \text{ (dynes)}_{\text{cgs}}}{\dot{x} \text{ (cm/sec)}_{\text{cgs}}}$$

Inductance:

$$E_{\text{(volts)}} = L_e \frac{dI}{dt} \left(\frac{\text{Amp}}{\text{sec}} \right)$$

$$F \text{ (dynes)} = M \text{ (grams)} \frac{d^2x}{dt^2} \left(\frac{\text{cm}}{\text{sec}^2} \right)$$

$$\& L_e = E \left(\right)$$

Capacitance